

A three-component model for the coupled evolution of near-inertial waves, quasi-geostrophic flow, and the near-inertial second harmonic

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We derive an asymptotic model that describes the nonlinear, coupled evolution of (i) near-inertial waves (NIWs), (ii) balanced quasi-geostrophic flow, and (iii) near-inertial second harmonic waves with frequency near $2f_0$, where f_0 is the local inertial frequency. This ‘three-component’ model extends the two-component model derived by Xie & Vanneste (*J. Fluid Mech.*, vol. 774, 2015, pp. 143–169) to include interactions between near-inertial and $2f_0$ waves. Both models possess two conservation laws which together imply that oceanic NIWs forced by winds, tides, or flow over bathymetry can extract energy from quasi-geostrophic flows. A second and separate implication of the three-component model is that quasi-geostrophic flow catalyzes a loss of NIW energy to freely propagating waves with near- $2f_0$ frequency that propagate rapidly to depth and transfer energy back to the NIW field at very small vertical scales. The upshot of near- $2f_0$ generation is a two-step mechanism whereby quasi-geostrophic flow catalyzes a nonlinear transfer of near-inertial energy to the small scales of wave breaking and diapycnal mixing. A comparison of numerical solutions to both Boussinesq and three-component models for a two-dimensional initial value problem reveals strengths and weakness of the model while demonstrating the extraction of quasi-geostrophic energy and production of small vertical scales.

1. Introduction

Near-inertial waves (NIWs) are inertia-gravity waves in rotating and stratified fluids with frequencies near the local inertial frequency, f_0 . In the oceans of Earth, an almost-universal strong density stratification means that NIWs have very small aspect ratios, large vertical shears, and the lowest of internal wave frequencies. Partly because of their small aspect ratios and low frequencies, oceanic NIWs are generated by such diverse processes as fluctuating winds and flow over topography, contain roughly half of the total internal wave kinetic energy, and are a main contributor to diapycnal mixing (Ferrari & Wunsch 2009).

The weak dispersion and slow propagation of NIWs exposes them to strong interaction with balanced quasi-geostrophic (QG) flows. A basic introduction to NIW propagation through non-uniform balanced flows is given by the WKB-based ray theories of Mooers (1975) and Kunze (1985), which show that near-inertial energy is attracted to regions of negative balanced vorticity and expelled from regions of positive vorticity. A more general theory valid both for ray-like NIW propagation and scattering by smaller-scale balanced

flows was developed by Young & Ben Jelloul (1997, YBJ hereafter). YBJ linearized the Boussinesq equations around a prescribed background flow and exploited weak near-inertial dispersion to develop a two-time asymptotic expansion that isolates the slow evolution of NIWs. The resulting YBJ NIW equation, which is similar to equation (1.8) below, describes the weakly dispersive propagation of β -plane NIWs through advecting and refracting balanced flows of near-arbitrary spatial structure.

The YBJ NIW equation successfully describes many aspects of near-inertial propagation through realistic balanced flows (Klein & Llewellyn Smith 2001; Klein, Llewellyn Smith & Lapeyre 2004; Danioux, Klein & Rivière 2008), but ignores nonlinear, finite-amplitude NIW dynamics and their corresponding feedback onto the balanced flow. In pursuit of a richer theory describing the coupled evolution of NIWs and balanced flows, Xie & Vanneste (2015, XV hereafter) derived a Generalized Lagrangian Mean model which joins the YBJ NIW equation to the quasi-geostrophic equations. Like Bühler & McIntyre (1998), Wagner & Young (2015), and as in equation (1.7) below, in the XV model an NIW-induced balanced flow takes part in advecting QG potential vorticity and thus in the evolution of QG flow.

1.1. The $2f_0$ harmonic and motivation for a three-component model

Both YBJ and XV lack a conspicuous aspect of NIW evolution observed in the kinetic energy frequency spectra of the Ocean Storms Experiment (D’Asaro *et al.* 1995), the observations of Niwa & Hibiya (1999), and in the simulations of NIW-QG interaction by Danioux *et al.* (2008): the nonlinear generation of internal waves with frequency $2f_0$. While the $2f_0$ waves have little horizontal kinetic energy relative to the NIWs, they can dominate the pressure field and contribute appreciably to vertical velocity and isopycnal displacement. Remarkably, $2f_0$ generation and subsequent horizontal radiation can remove energy from spatially compact regions of NIW-QG interaction, as discussed below and illustrated in figure 1. A primary motivation for this paper is the derivation of a more complete set of equations that contains the essential elements of YBJ and XV while including $2f_0$ waves. This derivation yields a model with three components: NIW velocity, balanced QG potential vorticity, and the amplitude of $2f_0$ pressure.

To motivate the three-component model, we consider an initial value problem in the Boussinesq equations in which a surface-concentrated NIW interacts with a balanced barotropic jet in two-dimensions (x, z) . We use a constant inertial frequency $f_0 = 10^{-4} \text{ s}^{-1}$ and buoyancy frequency $N = 2 \times 10^{-3} \text{ s}^{-1}$ associated with a stable background buoyancy profile. The velocity field is $\mathbf{u} = u\hat{\mathbf{x}} + v\hat{\mathbf{y}} + w\hat{\mathbf{z}}$ and the dynamic buoyancy perturbation from background is b , so that available potential energy density is $b^2/2N^2$. The initial v is a barotropic jet in geostrophic and hydrostatic balance flowing along the axis of y , while the initial u is a surface-concentrated, horizontally-uniform, and unbalanced flow which develops into a NIW. The balanced jet has the Gaussian profile

$$v(x, z, 0) = V_0 + V_1 \exp(-x^2/2L^2), \quad (1.1)$$

where V_0 is defined so that $v(x, z, 0)$ has zero horizontal average and thus no unbalanced component. The initial u is horizontally uniform and concentrated in a layer of depth h :

$$u(x, z, 0) = U_0 \exp(-z^2/2h^2). \quad (1.2)$$

The initial buoyancy b and vertical velocity w are zero. We solve this initial value problem in the Boussinesq equations using the spectral model of Winters, MacKinnon & Mills (2004) with 1536 Fourier modes in x and 768 sine/cosine modes in z .

If the jet in (1.1) were not present, the initial condition in u would develop into a horizontally uniform, non-propagating, perpetual inertial oscillation. Instead, refraction

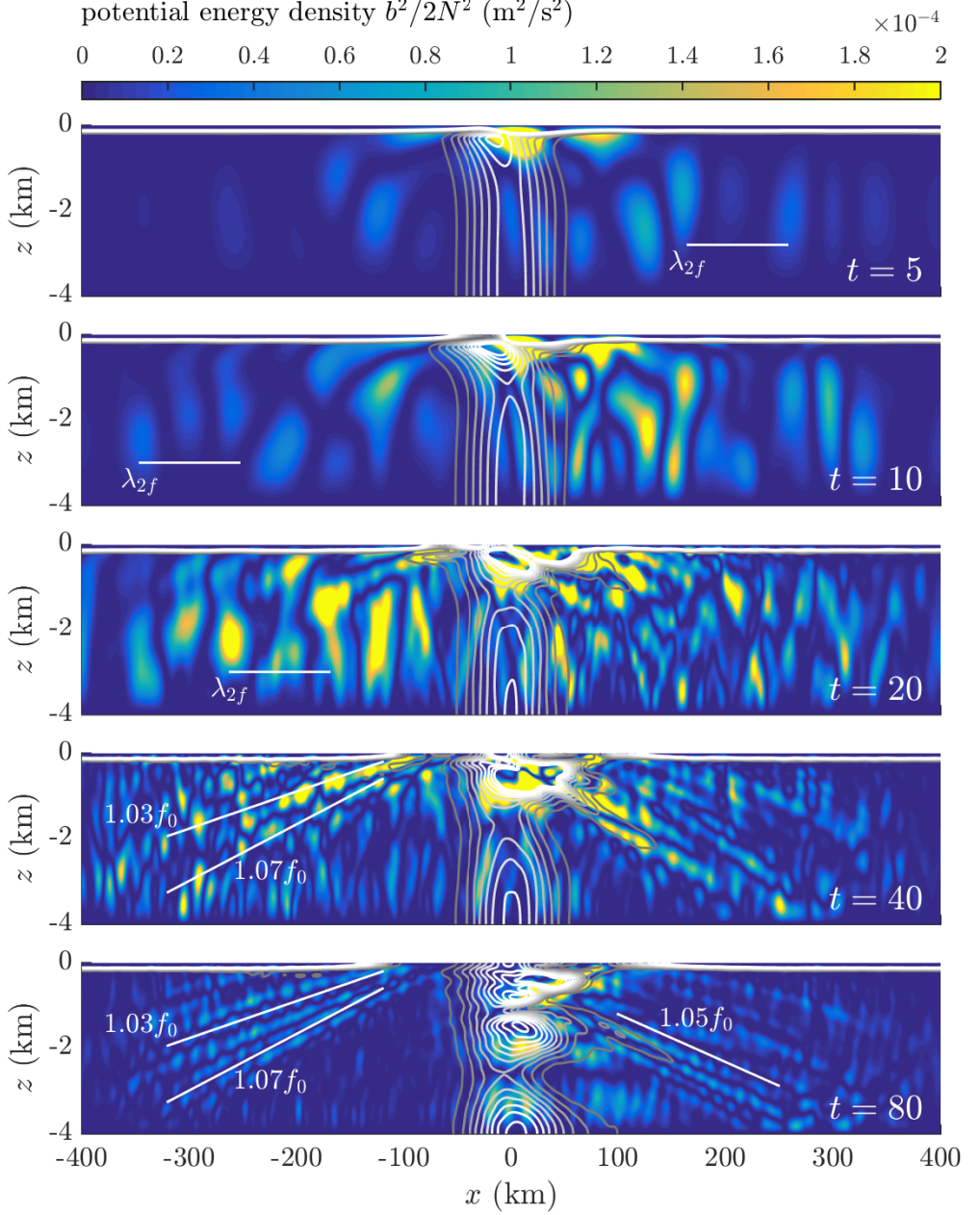


FIGURE 1. The numerical solution of a two-dimensional Boussinesq initial value problem involving the interaction between a barotropic jet and a surface-concentrated near-inertial wave (NIW). Shading shows potential energy density $b^2/2N^2$ and contours show kinetic energy density at 10 levels between 0.01 and $0.1 \text{ m}^2 \text{ s}^{-2}$ at $t = 5$ through $t = 80$ inertial periods. A horizontal line on the $t = 5$, 10 , and 20 snapshots shows the wavelength of a vertical mode-one $2f_0$ -frequency internal wave. The slanting lines on the $t = 40$ and $t = 80$ snapshots show the characteristic propagation angles of NIWs with the indicated frequencies. The initial v and u are given in (1.1) and (1.2), where $V_1 = 0.4 \text{ m s}^{-1}$, $L = 40 \text{ km}$, $U = 0.8 \text{ m s}^{-1}$, and $h = 100 \text{ m}$. Only the central 800 km of a 1200 km computational domain are shown. The solution is relaxed to a surface-concentrated inertial oscillation in sponge layers 150 km thick on the edges of the domain.

by the imposed jet injects small horizontal scales of size $\sim L$ into the NIW field, thus induces near-inertial vertical propagation and catalyzes radiation of low-mode $2f_0$ internal waves. The development of this process is illustrated in figure 1, which shows snapshots of potential energy density at $t = 5, 10, 20, 40$, and 80 inertial periods. The kinetic energy density is indicated by 10 overlain contours between 0.01 and $0.1 \text{ m}^2/\text{s}^2$. Throughout the simulation, kinetic energy remains localized in the surface layer and in the near-field of the barotropic jet. Bulges in kinetic energy appearing at $t = 20$ through 80 inertial periods reveal the progress of vertical NIW propagation and show how NIW energy is refractively focused into the region of negative vorticity (Lee & Niiler 1998; Balmforth, Llewellyn Smith & Young 1998; Balmforth & Young 1999).

The vertical propagation of NIW kinetic energy is attended by an evolving potential energy field. Its most conspicuous aspect is a signal that extends the full domain depth and radiates horizontally from the region of jet-NIW interaction. In early stages, the potential energy signal has vertical mode-one structure. A horizontal line on the panels at $t = 5, 10$ and 20 inertial periods indicates the horizontal wavelength $\lambda_{2f} = 2NH/\sqrt{3}f_0 = 92.4 \text{ km}$ of a mode-one, $2f_0$ frequency internal wave. Remarkably, while this $2f_0$ signal is generated by nonlinear NIW self-interaction in a small region, it rapidly radiates to fill a much larger volume without significant NIW activity (Danioux et al. 2008; Danioux & Klein 2008).

In addition to the low- and intermediate-mode $2f_0$ signal, narrow beams of potential energy radiate downwards and outwards from the center of the domain. These beams are NIWs propagating at the characteristic angles indicated by slanting lines on the snapshots at $t = 40$ and $t = 80$ inertial periods. The beams are produced by a scattering interaction between the surface-concentrated NIW and the jet. The rightward radiating beams are NIWs escaping the region of negative jet vorticity.

The two-dimensional NIW-jet interaction is thus characterized by at least three distinct phenomena: trapping of near-inertial energy in regions of negative balanced vorticity, beam-like radiation of near-inertial energy, and emission of $2f_0$ waves. We use a multiple space- and time-scale expansion of the Boussinesq equations to construct a three-component model describing all of these processes.

1.2. Summary of the three-component model

In the three-component model, the horizontal velocity is

$$u + iv \stackrel{\text{def}}{=} e^{-if_0t} LA + (-\partial_y + i\partial_x)\psi + \dots \quad (1.3)$$

where $A(x, y, z, t)$ is the NIW envelope and $\psi(x, y, z, t)$ is the quasi-geostrophic stream-function. The differential operator L in (1.3) is defined below in (1.7) and the \dots on the right of (1.3) stand for additional contributions to horizontal velocity: NIW harmonics, Stokes corrections, and ageostrophic flow. The pressure field is

$$p = f_0\psi + \frac{if_0}{2} \left[e^{-if_0t}(\partial_x - i\partial_y)A + e^{-2if_0t}2B \right] + \text{cc} + \dots, \quad (1.4)$$

where $B(x, y, z, t)$ is the $2f_0$ wave envelope, ‘cc’ stands for ‘complex conjugate’, and the \dots indicate unimportant high-order corrections. The vertical velocity w is

$$w = -\frac{f_0^2}{2N^2} \left[e^{-if_0t}(\partial_x - i\partial_y)A_z + e^{-2if_0t}4B_z \right] + \text{cc}. \quad (1.5)$$

The $2f_0$ contribution in B features prominently in the vertical velocity field, despite its small contribution to horizontal velocity.

The system consists of three equations: a wave-averaged quasi-geostrophic potential

vorticity equation, the NIW equation, and a ‘ $2f_0$ equation’ governing the evolution of $2f_0$ waves. The wave-averaged potential vorticity equation is

$$q_t + J(\psi, q) = 0, \quad (1.6)$$

where the potential vorticity is

$$q = \underbrace{\left(\partial_x^2 + \partial_y^2 + \partial_z \frac{f_0^2}{N^2} \partial_z \right)}_{\stackrel{\text{def}}{=} \Delta} \psi + \beta y + \underbrace{\frac{i}{2f_0} J(LA^*, LA)}_{\stackrel{\text{def}}{=} L} + \frac{1}{4f_0} \Delta |LA|^2. \quad (1.7)$$

In (1.6) and (1.7) the operator $J(a, b) = a_x b_y - a_y b_x$ is the Jacobian, the inertial of Coriolis frequency is $f = f_0 + \beta y$, and $N(z)$ is the depth-dependent buoyancy frequency associated with strong background stratification. The two rightmost terms in (1.7) are quadratic NIW contributions to the wave-averaged potential vorticity. We assume the $2f_0$ waves are too weak to contribute appreciably to potential vorticity. The evolution of the NIW field is described by a generalization of the YBJ equation,

$$LA_t + \frac{i}{2} f_0 \Delta A + J(\psi, LA) + iLA \left(\frac{1}{2} \Delta \psi + \beta y \right) + \frac{1}{2} LA^* (\partial_x + i\partial_y)^2 B = 0. \quad (1.8)$$

Equation (1.8) accounts for NIW dispersion and group propagation, horizontal advection by balanced flows, refraction by balanced flows and non-uniform planetary vorticity, and nonlinear NIW- $2f_0$ interaction. The NIW- $2f_0$ interaction term on the right end of (1.8) is identical to the term introduced by Young, Tsang, and Balmforth (2008) into the YBJ equation to analyze near-inertial parametric subharmonic instability (PSI); in that work, the NIW- $2f_0$ interaction was implicated in the production of very small NIW vertical scales.

The evolution of the $2f_0$ amplitude B is described by

$$(\Delta + 13L) B_t + 4if_0(\Delta - 3L)B = -\frac{3}{2}(\partial_x - i\partial_y)^2 (LA)^2. \quad (1.9)$$

Equation (1.9) describes dispersion and propagation of $2f_0$ waves and energy transfer from NIWs via the source term on the right.

The three-component model, comprised of equations (1.6) through (1.9), describes the coupled evolution of near-inertial waves, quasi-geostrophic flow, and near- $2f_0$ internal waves. Like the XV system, the three-component model conserves two integral quantities: ‘wave action’, and ‘coupled energy’. Wave action is a sum of NIW kinetic energy and the total energy of freely-propagating near- $2f_0$ waves. Coupled energy is the sum of total balanced energy, near-inertial potential energy, a NIW- β interaction term, and terms associated with the NIW- $2f_0$ interaction.

A striking implication of both the XV and three-component model is that NIWs can extract energy from balanced quasi-geostrophic flow. This follows from the separation of two conservation laws for wave action and coupled energy, which together imply that an increase in NIW potential energy during NIW-flow interaction comes at the expense of balanced energy. Balanced flow thus loses energy when interacting with NIWs that consist almost entirely of kinetic energy, and NIW-QG interaction forms a link between large-scale balanced energy, the energy contained in the internal wave field, and wave breaking and diapycnal mixing. XV refer to this wave-mean interaction as ‘stimulated loss-of-balance’ to distinguish it from spontaneous loss-of-balance (Vanneste 2013), emphasizing that it requires externally-forced waves to ‘stimulate’ further production of wave energy at the expense of balanced energy. Unlike spontaneous wave generation, stimulated wave generation is a potentially significant energy sink for nearly-balanced flows with small Rossby numbers.

Next in section 2, we introduce the Boussinesq equations, special scaling assumptions, and define the multiple time and multiple vertical scales required to meet solvability conditions in the asymptotic derivation. In section 3 we expand the Boussinesq equations in wave amplitude, deriving the NIW equation as well as the $2f_0$ equation governing the evolution of the $2f_0$ harmonic. In section 4 we apply the wave-averaged contribution to quasi-geostrophic potential vorticity found by Wagner & Young (2015) to the near-inertial case. In section 5 we heuristically revise the formal theory derived in sections 3 and 4 to arrive at the implementable model of equations (1.6) through (1.9). In section 6 we derive two conserved integral quantities from equations (1.6) through (1.9). In section 7 we compare numerical solutions of a two-dimensional initial value problem in both Boussinesq and three-component models, and in section 8 we assess the solutions' physical implications. We conclude with a discussion of the model's significance and implications in section 9.

2. The Boussinesq equations

We use the Boussinesq approximation by defining a constant reference density ρ_0 and decomposing the total density into

$$\rho(\mathbf{x}, t) = \rho_0 \left[1 + g^{-1} \int_z^0 N^2(z') dz' - g^{-1} b(\mathbf{x}, t) \right], \quad (2.1)$$

where $\mathbf{x} = (x, y, z)$ is position and t is time. In (2.1), the resting buoyancy profile is the vertical integral of the buoyancy frequency $N^2(z)$, and $b(\mathbf{x}, t)$ is the dynamic buoyancy perturbation from background. Pressure is decomposed similarly into $-\rho_0 g z + \rho_0 P(z) + \rho_0 p(\mathbf{x}, t)$, where $P(z)$ is the resting hydrostatic pressure and the dynamic component of pressure is $\rho_0 p$.

Using these definitions, the Boussinesq equations are

$$u_t + \mathbf{u} \cdot \nabla u - f v + p_x = 0, \quad (2.2)$$

$$v_t + \mathbf{u} \cdot \nabla v + f u + p_y = 0, \quad (2.3)$$

$$w_t + \mathbf{u} \cdot \nabla w + p_z = b, \quad (2.4)$$

$$b_t + \mathbf{u} \cdot \nabla b + w N^2 = 0, \quad (2.5)$$

$$u_x + v_y + w_z = 0, \quad (2.6)$$

where $\mathbf{u} = u\hat{\mathbf{x}} + v\hat{\mathbf{y}} + w\hat{\mathbf{z}}$ is the fluid velocity. Subscripts with respect to (x, y, z) or t denote partial derivatives. We use the beta-plane approximation by introducing $f(y) = f_0 + \beta y$, where f_0 is the local inertial frequency and β its latitudinal variation.

2.1. Non-dimensionalization and scaling assumptions

We set the asymptotic reduction in motion by non-dimensionalizing the Boussinesq equations (2.2) through (2.6). We choose a spatial scaling that isolates NIWs at leading-order and a velocity scaling that ensures the back-rotated velocity and the QG potential vorticity share the same evolutionary time scale. Specifically, this requires that NIW dispersion acts on the same time scale as advection and refraction by the balanced flow. We use a single horizontal length scale, L , and denote the scale of the near-inertial horizontal velocity with \tilde{U} . The NIW ‘amplitude parameter’

$$\epsilon \stackrel{\text{def}}{=} \frac{\tilde{U}}{f_0 L}, \quad (2.7)$$

is crucial: $\epsilon \ll 1$ implies nonlinear terms are small so that the NIW field is governed by linear dynamics to leading-order.

The amplitude and importance of nonlinearity to balanced flow evolution is measured by the Rossby number. We assume the balanced flow is weak relative to the near-inertial waves and that $\bar{U} = \epsilon \tilde{U}$, where \bar{U} is the characteristic velocity of the balanced flow. Under this scaling assumption the Rossby number is

$$Ro \stackrel{\text{def}}{=} \frac{\bar{U}}{f_0 L} = \epsilon^2. \quad (2.8)$$

The NIW amplitude parameter and Rossby number have superficial similarity but different physical interpretations. The NIW amplitude can be interpreted as the ratio between the length scale L and the radius of particle orbits in an inertial circle, \tilde{U}/f_0 . The Rossby number, on the other hand, is the ratio of the rotation time scale $1/f_0$ and advective time scale $L/\bar{U} = (\epsilon^2 f_0)^{-1}$. The NIW envelope and the balanced flow co-evolve on the slow time scale $(\epsilon^2 f_0)^{-1}$.

We denote the vertical scale of the near-inertial waves by \tilde{H} and we use \tilde{U} , L , and \tilde{H} to non-dimensionalize the horizontal and vertical velocities,

$$(u, v) = \tilde{U} (\tilde{u}, \tilde{v}), \quad w = \frac{\tilde{H} \tilde{U}}{L} \tilde{w}, \quad (2.9)$$

where non-dimensional variables are distinguished by $\tilde{\cdot}$. Introducing f_0 , the local Coriolis or inertial frequency, and N_0 , the characteristic magnitude of $N(z)$, we non-dimensionalize the buoyancy field with

$$b = \left(\tilde{H} N_0^2 \tilde{U} / f_0 L \right) \tilde{b}. \quad (2.10)$$

We adopt a geostrophic scaling for the pressure such that

$$p = f_0 L \bar{U} \tilde{p} = \epsilon f_0 L \tilde{U} \tilde{p}. \quad (2.11)$$

The inertial frequency is scaled so that

$$\tilde{f} = 1 + \epsilon^2 \tilde{\beta} \tilde{y}, \quad (2.12)$$

where $(x, y) = L(\tilde{x}, \tilde{y})$ and

$$\tilde{\beta} = \frac{\beta L^2}{\bar{U}}. \quad (2.13)$$

Finally, we define an aspect ratio

$$\alpha \stackrel{\text{def}}{=} \epsilon \frac{N_0}{f_0}. \quad (2.14)$$

By assuming $\alpha = O(1)$, we imply that $f_0/N_0 = O(\epsilon)$ and justify the hydrostatic approximation in the vertical momentum equation at all relevant orders in the perturbation theory.

2.2. Multiple scales: time and space

To describe both internal waves and slowly evolving balanced flow, we use the two-time method with a ‘fast’ time $\tilde{t} = f_0 t$, and a ‘slow’ time $\bar{t} = \epsilon^2 f_0 t$. Time-derivatives are mapped according to

$$\partial_t \mapsto f_0 \left(\partial_{\tilde{t}} + \epsilon^2 \partial_{\bar{t}} \right). \quad (2.15)$$

We use an Eulerian time-average denoted with an overbar and defined as

$$\bar{\phi}(\mathbf{x}, \bar{t}) \stackrel{\text{def}}{=} \frac{1}{T} \int_{t-T/2}^{t+T/2} \phi(\mathbf{x}, t') dt', \quad \text{where} \quad \frac{1}{f_0} \ll T \ll \frac{L}{U}, \quad (2.16)$$

to separate fast and slow flow components. Thus any field ϕ can be represented as

$$\phi = \bar{\phi} + \tilde{\phi}, \quad (2.17)$$

where $\bar{\phi}$ is the slowly evolving time-mean part and $\tilde{\phi}$ is the wavy part with $\bar{\tilde{\phi}} = 0$.

A multiple-vertical-scale expansion in the vertical is motivated by the disparity in aspect ratio between NIWs, and both observed $2f_0$ scales as well as standard quasi-geostrophic flow. Denoting the vertical scale of the NIWs by \tilde{H} , the internal-wave dispersion relation implies that internal waves are near-inertial when the Burger number of the wave is small, or when

$$\left(\frac{N_0 \tilde{H}}{f_0 L} \right)^2 \ll 1. \quad (2.18)$$

On the other hand, the standard quasi-geostrophic equations assume that the Burger number of the balanced flow is order unity. We use this requirement to define the vertical scale of the balanced flow, \bar{H} , as

$$\bar{H} \stackrel{\text{def}}{=} \frac{f_0 L}{N_0}. \quad (2.19)$$

We make the scaling assumption that

$$\tilde{H} = \epsilon \bar{H}. \quad (2.20)$$

This prescription for \tilde{H} unifies the slow NIW dispersion time scale with the balanced-flow advection time scale. To capture both vertical scales in the expansion we split the vertical coordinate into a fast component, \tilde{z} , and a slow component, \bar{z} . Under this two-scale splitting, vertical derivatives become

$$\partial_z \mapsto \tilde{H}^{-1} (\partial_{\tilde{z}} + \epsilon \partial_{\bar{z}}). \quad (2.21)$$

The vertical-scale splitting requires the introduction of a vertical average, which we define as

$$\hat{\phi} = \frac{1}{H'} \int_{\bar{z}-H'/2}^{\bar{z}+H'/2} \phi d\tilde{z}', \quad \text{where} \quad \tilde{H} \ll H' \ll \bar{H}. \quad (2.22)$$

The increase in complexity incurred by the multiple space-scale expansion is justified by a systematic explanation of the prominence and impact of the $2f_0$ harmonic on NIW evolution.

2.3. Complexified non-dimensionalized equations

The derivation is greatly simplified by defining the complex horizontal coordinate and velocity field,

$$s \stackrel{\text{def}}{=} x + iy, \quad \text{and} \quad \mathcal{U} \stackrel{\text{def}}{=} u + iv. \quad (2.23)$$

Spatial derivatives are expressed in terms of s and s^* via

$$\partial_s = \frac{1}{2} (\partial_x - i\partial_y), \quad \partial_{s^*} = \frac{1}{2} (\partial_x + i\partial_y). \quad (2.24)$$

These imply that $\Delta = 4\partial_s \partial_{s^*}$, and that

$$u_x + v_y = \mathcal{U}_s + \mathcal{U}_{s^*}^* \quad \text{and} \quad v_x - u_y = i\mathcal{U}_{s^*}^* - i\mathcal{U}_s. \quad (2.25)$$

Using the scaling assumptions outlined above, and dropping decorations on non-dimensional variables, the complexified, non-dimensional Boussinesq equations become

$$\mathcal{U}_{\bar{t}} + i\mathcal{U} = -\epsilon(\mathbf{u} \cdot \nabla \mathcal{U} + 2p_{s*}) - \epsilon^2(\mathcal{U}_{\bar{t}} + w\mathcal{U}_{\bar{z}} + i\beta y\mathcal{U}), \quad (2.26)$$

$$p_{\bar{z}} = \epsilon(b - p_{\bar{z}}) - \epsilon^2\alpha^{-2}\left[w_{\bar{t}} + \epsilon(\mathbf{u} \cdot \nabla w) + \epsilon^2(w w_{\bar{z}} + w_{\bar{t}})\right], \quad (2.27)$$

$$b_{\bar{t}} + wN^2 = -\epsilon\mathbf{u} \cdot \nabla b - \epsilon^2(b_{\bar{t}} + w b_{\bar{z}}), \quad (2.28)$$

$$\mathcal{U}_s + \mathcal{U}_{s*}^* + w_{\bar{z}} = -\epsilon w_{\bar{z}}. \quad (2.29)$$

The bracketed terms in (2.27) are included for completeness, but never appear in the theory that follows. In terms of complex velocity the advection operators in (2.26) and (2.28) are

$$\mathbf{u} \cdot \nabla = \mathcal{U}\partial_s + \mathcal{U}^*\partial_{s*} + w\partial_{\bar{z}}. \quad (2.30)$$

The system in (2.26) through (2.29) is the basis for our asymptotic derivation.

3. The NIW equation

The NIW equation is derived by developing a perturbation expansion of (2.26) through (2.29) for $\epsilon \ll 1$. We begin by expanding \mathbf{u} , b , and p each in a series in ϵ . For example, the complex velocity \mathcal{U} has the expansion

$$\mathcal{U} = \mathcal{U}_0 + \epsilon \mathcal{U}_1 + \epsilon^2 \mathcal{U}_2 + \dots. \quad (3.1)$$

We develop equations (2.26) through (2.29) order-by-order in ϵ . For clarity, we express our results in dimensional variables, though the non-dimensional forms are indispensable for distinguishing each order in the development.

3.1. Leading order: near-inertial waves

The leading-order terms in (2.26) through (2.29) are

$$\mathcal{U}_{0\bar{t}} + if_0\mathcal{U}_0 = 0, \quad (3.2)$$

$$p_{0\bar{z}} = 0, \quad (3.3)$$

$$b_{0\bar{t}} + w_0N^2 = 0, \quad (3.4)$$

$$\mathcal{U}_{0s} + \mathcal{U}_{0s*}^* + w_{0\bar{z}} = 0. \quad (3.5)$$

We write the solution to the horizontal momentum equation (3.2) in terms of an NIW envelope M or A ,

$$\mathcal{U}_0 = e^{-if_0\bar{t}} M_{\bar{z}} = e^{-if_0\bar{t}} \tilde{L}A, \quad (3.6)$$

where \tilde{L} is a second-order differential operator

$$\tilde{L} \stackrel{\text{def}}{=} \partial_{\bar{z}} \left(\frac{f_0^2}{N^2} \partial_{\bar{z}} \right). \quad (3.7)$$

Both $A(x, y, \bar{z}, \bar{t})$ and $M = (f_0^2/N^2)A_{\bar{z}}$ prove useful for confronting the algebra that ensues. The representation in (3.6) ensures the leading-order horizontal velocity is inertial over short times; small deviations in wave field frequency from f_0 are captured by the dependence of M or A on the slow time \bar{t} . The construction in (3.6) also implies that the vertical average of the NIW horizontal velocity is zero at this order.

With the representation in (3.6), we can integrate the continuity equation (3.5) over

the fast vertical coordinate \tilde{z} to yield

$$w_0 = -e^{-if_0\tilde{t}}M_s - e^{if_0\tilde{t}}M_{s^*}^* + \hat{w}_0, \quad (3.8)$$

where the \tilde{z} -independent function of integration $\hat{w}_0(x, y, \bar{z}, \tilde{t}, \bar{t})$ is necessary to ensure solvability of the perturbation expansion at next order. If \hat{w}_0 is not included in (3.8) then the $O(\epsilon)$ velocity field cannot satisfy continuity and the boundary conditions. At $O(\epsilon)$ in equations (2.26) through (2.29), we find that \hat{w}_0 oscillates on the fast time with frequency $2f_0$ and is forced nonlinearly by NIW horizontal self-advection.

The leading-order buoyancy b_0 follows from integration of the buoyancy equation (3.4) using w_0 in (3.8),

$$b_0 = if_0 \left(e^{-if_0\tilde{t}}A_{\tilde{z}s} - e^{if_0\tilde{t}}A_{\tilde{z}s^*}^* \right) + \hat{b}_0, \quad (3.9)$$

where as in (3.8) we include the function of integration $\hat{b}_0(x, y, \bar{z}, \tilde{t}, \bar{t})$. The vertical momentum equation (3.3) implies that the leading-order pressure p_0 does not depend on the fast vertical scale \tilde{z} , or that

$$p_0 = \hat{p}_0. \quad (3.10)$$

The leading-order pressure p_0 is eventually determined by (3.28) and (3.29) below and oscillates on a fast time-scale with frequency $2f_0$. An important feature eventually revealed by this expansion is that the large-vertical-scale $2f_0$ fields \hat{w}_0 , \hat{b}_0 and \hat{p}_0 appear at leading order in (3.8), (3.9) and (3.28). The magnitudes of these $2f_0$ fields follows from the two assumptions that $2f_0$ horizontal velocity and vertical scales are respectively $O(\epsilon)$ and $O(\epsilon^{-1})$ compared to their near-inertial counterparts. This scaling produces a description of NIW- $2f_0$ interaction that neglects the complicating effect of the mean flow ψ on $2f_0$ evolution.

3.2. First order: wave-averaged geostrophic balance and $2f_0$ harmonic

The $O(\epsilon)$ terms in equations (2.26) through (2.29) are

$$\mathcal{U}_{1\tilde{t}} + if_0\mathcal{U}_1 = -2p_{0s^*} - \mathbf{u}_0 \cdot \nabla \mathcal{U}_0, \quad (3.11)$$

$$p_{1\tilde{z}} = b_0 - p_{0\tilde{z}}, \quad (3.12)$$

$$b_{1\tilde{t}} + w_1 N^2 = -\mathbf{u}_0 \cdot \nabla b_0, \quad (3.13)$$

$$\mathcal{U}_{1s} + \mathcal{U}_{1s^*}^* + w_{1\tilde{z}} = -w_{0\tilde{z}}. \quad (3.14)$$

These equations describe wave-averaged geostrophic balance and the nonlinearly forced $2f_0$ harmonic.

3.2.1. Wave-averaged geostrophic balance

The time-average of (3.11) through (3.14) yields the wave-averaged geostrophic balance conditions. These balance conditions are similar to those in Wagner & Young (2015) except that the restriction to NIWs means there is no Stokes pressure contribution. We show this explicitly by first noting that the nonlinear term on the right hand side of (3.11) is

$$\mathbf{u}_0 \cdot \nabla \mathcal{U}_0 = \mathcal{J}_0 + e^{-2if_0\tilde{t}}\mathcal{J}_2 + e^{-if_0\tilde{t}}\hat{w}_0 M_{\tilde{z}\tilde{z}}, \quad (3.15)$$

where \mathcal{J}_0 and \mathcal{J}_2 are Jacobians defined by

$$\mathcal{J}_0 \stackrel{\text{def}}{=} \frac{\partial(M^*, M_{\tilde{z}})}{\partial(\tilde{z}, s^*)}, \quad \text{and} \quad \mathcal{J}_2 \stackrel{\text{def}}{=} \frac{\partial(M, M_{\tilde{z}})}{\partial(\tilde{z}, s)}. \quad (3.16)$$

Next, we observe that the horizontal and vertical Stokes drift, \mathcal{U}^S and w^S , are defined

$$\mathcal{U}^S \stackrel{\text{def}}{=} \overline{\boldsymbol{\xi}_0 \cdot \nabla \mathcal{U}_0}, \quad \text{and} \quad w^S \stackrel{\text{def}}{=} \overline{\boldsymbol{\xi}_0 \cdot \nabla w_0}, \quad (3.17)$$

where $\boldsymbol{\xi}_0 = \xi_0 \hat{\mathbf{x}} + \eta_0 \hat{\mathbf{y}} + \zeta_0 \hat{\mathbf{z}}$ is the wave particle displacement, defined via $\boldsymbol{\xi}_{0\tilde{t}} = \mathbf{u}_0$ and $\boldsymbol{\xi}_0 = 0$. A direct calculation shows that

$$\text{if}_0 \mathcal{U}^S = \overline{\mathbf{u}_0 \cdot \nabla \mathcal{U}_0} = \mathcal{J}_0. \quad (3.18)$$

A similar calculation for the vertical Stokes drift w^S shows that

$$\text{if}_0 w^S = \frac{\text{if}_0}{N^2} \overline{\mathbf{u}_0 \cdot \nabla b_0} = \mathcal{K}_0^* - \mathcal{K}_0, \quad (3.19)$$

where \mathcal{K}_0 is the Jacobian

$$\mathcal{K}_0 \stackrel{\text{def}}{=} \frac{\partial (M^*, M_s)}{\partial (\tilde{z}, s^*)}. \quad (3.20)$$

The identity $\mathcal{J}_{0s} + \mathcal{J}_{0s^*}^* + \mathcal{K}_{0z}^* - \mathcal{K}_{0z} = 0$ implies that the three-dimensional Stokes velocity in (3.18) and (3.19) is non-divergent.

Defining the quasi-geostrophic streamfunction as

$$\psi \stackrel{\text{def}}{=} \frac{\bar{p}_0}{f_0}, \quad (3.21)$$

we use the expressions for the Stokes velocities in (3.18) and (3.19) to write the time average of (3.11) and (3.13) as

$$\bar{\mathcal{U}}_1 + \mathcal{U}^S = 2\text{i}\psi_{s^*}, \quad (3.22)$$

$$\bar{w}_1 + w^S = 0. \quad (3.23)$$

Equation (3.22) is the wave-averaged geostrophic balance condition for quasi-geostrophic flow evolution in a field of strong NIWs. This balance condition lacks the Stokes pressure correction term that appears in the more general balance condition expressed by equation (4.38) in Wagner & Young (2015). From the leading-order vertical momentum equations (3.3), the pressure p_0 , and therefore ψ , does not depend on the fast vertical coordinate \tilde{z} .

3.2.2. The $2f_0$ harmonic

Using the two-time decomposition in (2.17), we write the wavy part of the first-order equations (3.11), (3.12), and (3.14),

$$\tilde{\mathcal{U}}_{1\tilde{t}} + \text{if}_0 \tilde{\mathcal{U}}_1 + 2\tilde{p}_{0s^*} = -e^{-2\text{i}f_0\tilde{t}} \mathcal{J}_2 - e^{-\text{i}f_0\tilde{t}} \hat{w}_0 M_{\tilde{z}\tilde{z}} \quad (3.24)$$

$$\tilde{p}_{1\tilde{z}} = \tilde{b}_0 - \tilde{p}_{0\tilde{z}}, \quad (3.25)$$

$$\hat{b}_{0\tilde{t}} + \hat{w}_0 N^2 = 0, \quad (3.26)$$

$$\tilde{\mathcal{U}}_{1s} + \tilde{\mathcal{U}}_{1s^*}^* + \tilde{w}_{1\tilde{z}} = -\tilde{w}_{0\tilde{z}}, \quad (3.27)$$

where with (3.26) we include the vertically-averaged, leading-order buoyancy equation. It is (3.26), rather than the wavy part of (3.13), which describes the part of the $2f_0$ buoyancy field with large vertical scale. Note that the final term on the right of equation (3.24) is not resonant because \hat{w}_0 oscillates with $2f_0$ frequency.

The system in (3.24) through (3.27) provides a complete description of the $2f_0$ harmonic of the NIW field. Importantly, part of this $2f_0$ -harmonic response does not depend on the fast vertical coordinate \tilde{z} . To isolate the slowly vertically-varying part of the $2f_0$ harmonic we average (3.24) through (3.27) over \tilde{z} and wrangle the resulting

system into a single equation. We leave the details to Appendix A and note the final result. Using the notation

$$\tilde{p}_0 = if_0 \left[e^{-2if_0\tilde{t}} B(x, y, \bar{z}, \bar{t}) - e^{2if_0\tilde{t}} B^*(x, y, \bar{z}, \bar{t}) \right], \quad (3.28)$$

we find that B solves

$$if_0 (\Delta - 3\bar{L}) B = -\frac{3}{2} \partial_s^2 \widehat{M_z^2}. \quad (3.29)$$

The operator \bar{L} is a second-order differential operator analogous to \tilde{L} but defined in terms of the slow vertical scale \bar{z} ,

$$\bar{L} \stackrel{\text{def}}{=} \partial_{\bar{z}} \frac{f_0^2}{N^2} \partial_{\bar{z}}. \quad (3.30)$$

The ‘ $2f_0$ equation’ in (3.29) describes forced $2f_0$ oscillations with a much larger vertical scale than the near-inertial fields. Because of this vertical-scale discrepancy, the vertical velocity of the $2f_0$ -harmonic appears alongside the NIW vertical velocity at leading-order in (3.8). As it stands, however, equation (3.29) cannot describe freely-propagating $2f_0$ waves and thus cannot describe the waves which produce the prominent potential energy signal in figure 1. We modify (3.29) heuristically in section 5 to describe the freely-propagating parts of B , which roughly satisfy the $2f_0$ dispersion relation and thus obey $\Delta B \approx 3LB$.

Continuing with the derivation of the NIW evolution equation, we use the expression for \tilde{p}_0 in equation (3.28) to integrate (3.24) for $\tilde{\mathcal{U}}_1$. The full \mathcal{U}_1 field is

$$\mathcal{U}_1 = 2i\psi_{s^*} + if_0^{-1} \mathcal{J}_0 + e^{-2if_0\tilde{t}} (2B_{s^*} - if_0^{-1} \mathcal{J}_2) + \frac{2}{3} e^{2if_0\tilde{t}} B_{s^*}^* + \dots \quad (3.31)$$

where \dots indicates terms proportional to $e^{-3if_0\tilde{t}}$ and $e^{if_0\tilde{t}}$. Finally, we find $p_1 - \hat{p}_1$ by subtracting the vertical average from (3.25), using (3.9), and integrating in \bar{z} to find

$$p_1 - \hat{p}_1 = if_0 \left(A_s e^{-if_0\tilde{t}} - A_{s^*}^* e^{if_0\tilde{t}} \right). \quad (3.32)$$

We now have \mathcal{U}_1 , \hat{w}_0 , and p_1 and are ready to proceed to the second-order system.

3.3. Second order: an NIW amplitude evolution equation

The $O(\epsilon^2)$ terms in the horizontal momentum equation (2.26) are

$$\mathcal{U}_{2\tilde{t}} + if_0 \mathcal{U}_2 = -\mathbf{u}_0 \cdot \nabla \mathcal{U}_1 - \mathbf{u}_1 \cdot \nabla \mathcal{U}_0 - \mathcal{U}_{0\tilde{t}} - i\beta y \mathcal{U}_0 - 2p_{1s^*} - w_0 \mathcal{U}_{0\bar{z}}, \quad (3.33)$$

Here we finally apply the solvability condition arising from the introduction of multiple time scales. The solvability condition prevents the disordering of terms that would result from secular growth in \mathcal{U}_2 : we isolate resonant forcing terms on the right of (3.33) and set them collectively to zero. The amplitude equation yielded by this procedure governs the dependence of the NIW envelope A on the slow time \tilde{t} . We note that the vertical average of (3.33) has no resonant terms.

We construct the amplitude equation piece by piece, starting at the far-right end of (3.33) and proceeding to the left. The final term $w_0 \mathcal{U}_{0\bar{z}}$ in (3.33) has no parts proportional to $e^{-if_0\tilde{t}}$ and so does not contribute to the amplitude equation. The next three terms from the left side of (3.33) are

$$\mathcal{U}_{0\tilde{t}} + i\beta y \mathcal{U}_0 + 2\partial_{s^*} (p_1 - \hat{p}_1) = e^{-if_0\tilde{t}} \left(\tilde{L} A_{\tilde{t}} + i\beta y \tilde{L} A + 2if_0 A_{ss^*} \right) + \text{NRT}, \quad (3.34)$$

where NRT stands for ‘non-resonant terms’. Next in line is

$$(\mathbf{u}_1 \cdot \nabla) \mathcal{U}_0 = e^{-if_0 \tilde{t}} \left[2i \frac{\partial(\psi, M_{\tilde{z}})}{\partial(s^*, s)} - \mathcal{U}^S M_{\tilde{z}s} - \mathcal{U}^{S*} M_{\tilde{z}s^*} - w^S M_{\tilde{z}\tilde{z}} \right] + \text{NRT}. \quad (3.35)$$

Note that to find (3.35) we need only consider the time-mean velocity $\bar{\mathbf{u}}_1$, since \mathcal{U}_0 is proportional to $e^{-if_0 \tilde{t}}$. The first term on the right of (3.33), involving the zero-order advection of the first-order velocity, is the most complicated. Carefully compiling the terms, we find

$$(\mathbf{u}_0 \cdot \nabla) \mathcal{U}_1 = e^{-if_0 \tilde{t}} \left(M_{\tilde{z}} \mathcal{U}_{1s} - M_s \mathcal{U}_{1\tilde{z}} \right) + e^{if_0 \tilde{t}} \left(M_{\tilde{z}}^* \mathcal{U}_{1s^*} - M_{s^*}^* \mathcal{U}_{1\tilde{z}} \right) + \hat{w}_0 \mathcal{U}_{1\tilde{z}}, \quad (3.36)$$

$$= e^{-if_0 \tilde{t}} \left[\frac{\partial(M, \bar{\mathcal{U}}_1)}{\partial(\tilde{z}, s)} + \frac{i}{f_0} \frac{\partial(\mathcal{J}_2, M^*)}{\partial(\tilde{z}, s^*)} + 2M_{\tilde{z}}^* B_{s^*s^*} \right] + \text{NRT}. \quad (3.37)$$

Adding (3.35) to (3.37) yields

$$(\mathbf{u}_1 \cdot \nabla) \mathcal{U}_0 + (\mathbf{u}_0 \cdot \nabla) \mathcal{U}_1 = e^{-if_0 \tilde{t}} \left[2i \frac{\partial(\psi, M_{\tilde{z}})}{\partial(s^*, s)} + 2i\psi_{ss^*} M_{\tilde{z}} + 2M_{\tilde{z}}^* B_{s^*s^*} \right] + \text{NRT}. \quad (3.38)$$

The absence of terms cubic in M is a remarkable aspect of (3.38): all sixteen cubic- M terms in (3.35) and (3.37) conspire in collective cancellation. This simplification was previously noted by Falkovich *et al.* (1994) and Zeitlin *et al.* (2003), and is the reason why no cubic terms appear in XV.

It is thus notable that our expansion identifies a surviving ‘honorary’ cubic term, proportional to $M_{\tilde{z}}^* B_{s^*s^*}$, in (3.38). This new term results from the interaction of NIWs with both forced and freely-propagating $2f_0$ waves. The requirement for $2f_0$ fields arises when the first-order continuity equation (3.27) is averaged over the small NIW vertical scale: if the vertical average of $\mathcal{U}_{1s} + \mathcal{U}_{1s^*}^*$ is non-zero, for example, then continuity can only be satisfied if \mathcal{U}_1 is permitted its own independent evolution. This solvability issue is addressed by introducing the $2f_0$ fields \hat{w}_0 , \hat{b}_0 and \hat{p}_0 at leading order in (3.8) and (3.9). This is the non-obvious step that ultimately produces the new term in (3.38).

The amplitude equation is then obtained from the sum of (3.34) and (3.38). In Cartesian coordinates and in terms of A , the amplitude equation is

$$\tilde{L}A_{\tilde{t}} + \frac{if_0}{2} \triangle A + J(\psi, \tilde{L}A) + i\tilde{L}A \left(\frac{1}{2} \triangle \psi + \beta y \right) + \frac{1}{2} \tilde{L}A^* (\partial_x + i\partial_y)^2 B = 0. \quad (3.39)$$

The amplitude equation (3.39) is the YBJ equation except for the final $2f_0$ interaction term on the left hand side. The $2f_0$ interaction term is identical to the one found by Young *et al.* (2008) in their analysis of energy transfer from prescribed $2f_0$ motions to NIWs by parametric subharmonic instability (PSI).

4. The NIW-averaged available potential vorticity

Wave-averaged quasi-geostrophic flow is governed by a wave-averaged potential vorticity equation (Bühler & McIntyre 1998; Wagner & Young 2015),

$$q_{\tilde{t}} + J(\psi, q) = 0, \quad (4.1)$$

where ψ is defined through the balance condition (3.22) and q is the wave-averaged available potential vorticity. Wagner & Young (2015) give a number of expressions for q .

Here, we use

$$q \stackrel{\text{def}}{=} (\Delta + L)\psi + \beta y + \underbrace{\overline{J(u_0, \xi_0)} + \overline{J(v_0, \eta_0)} + f_0 \overline{J(\xi_0, \eta_0)} + \frac{1}{2} \left(\overline{\xi_{0i} \xi_{0j}} \right)_{,ij}}_{\stackrel{\text{def}}{=} q^w}. \quad (4.2)$$

In (4.2) we define the wave contribution to available potential vorticity, q^w , in terms of the leading-order wave particle displacement $\xi_0 = \xi_0 \hat{x} + \eta_0 \hat{y} + \zeta_0 \hat{z}$ defined through $\xi_{0\tilde{t}} = \mathbf{u}_0$.

In the present multiple-scale theory, ψ and q are both time-averaged and vertically-averaged quantities. Consistency then demands that q^w in (4.2) be vertically averaged as well. With the leading-order wave expressions (3.6) and (3.8) and using M , a bit of algebra leads to

$$q^w = -\frac{1}{f_0} (M_{ss}^* M_{\tilde{z}\tilde{z}} - 2M_{\tilde{z}s}^* M_{\tilde{z}s}^* + M_{ss}^* M_{\tilde{z}\tilde{z}}^*). \quad (4.3)$$

This is the expression for q^w found by XV.

We then take the vertical average of q^w , which yields a number of representations via integration by parts in \tilde{z} , such as

$$\widehat{q^w} = -\frac{1}{f_0} \left(\widehat{M_{ss}^* M_{\tilde{z}\tilde{z}}} - 2\widehat{M_{\tilde{z}s}^* M_{\tilde{z}s}^*} + \widehat{M_{ss}^* M_{\tilde{z}\tilde{z}}^*} \right), \quad (4.4)$$

$$= \frac{i}{2f_0} \overline{J(M_{\tilde{z}}^*, M_{\tilde{z}})} + \frac{1}{4f_0} \Delta \overline{|M_{\tilde{z}}|^2}. \quad (4.5)$$

We take the second form, in (4.5), which is the form needed to furnish the three-component model in (1.6) through (1.9) with a coupled wave-mean energy conservation law.

5. Remodeling

The formally-derived model comprised of (3.39), (4.2), (4.5) and (3.29) is a first draft that we heuristically revise to obtain the simpler and well-posed system in (1.6) through (1.9). This remodeling addresses two concerns with the multiple-scale formulation. First, the multiple vertical scales and vertical averages in (4.5) and (3.29) complicate computations. Second, the $2f_0$ equation in (3.29) cannot be solved when the NIW field and its $2f_0$ harmonic interact resonantly, which occurs when the nonlinear forcing on the right hand side of (3.29) has spectral components in the null space of the operator $\Delta - 3L$ on the left.

To address the first concern we reconsolidate vertical scales and eliminate vertical averaging from equations (4.5) and (3.29). Though this modification admits spurious small vertical scales into ψ and B , these small-scale parts of ψ and B contain little energy due to the ‘self-averaging’ Helmholtzian inversions that determine ψ and B through (4.2) and (3.29). In particular, energy is transferred most effectively to B at resonant or near-resonant spectral components of (3.29) and (5.3). These spectral components lie close to the $2f_0$ dispersion relation and have large vertical scale relative to NIWs.

After consolidation of scales and dismissal of vertical averages the potential vorticity is given in terms of ψ and wave-averaged properties as

$$q = (\Delta + L)\psi + \frac{i}{2f_0} J(LA^*, LA) + \frac{1}{4f_0} \Delta |LA|^2, \quad (5.1)$$

and the NIW equation is

$$LA_t + \frac{i}{2} f_0 \Delta A + J(\psi, LA) + iLA(\frac{1}{2}\Delta\psi + \beta y) + \frac{1}{2} LA^*(\partial_x + i\partial_y)^2 B = 0. \quad (5.2)$$

Above $L = \partial_z f_0^2 / N^2 \partial_z$ is the operator originally defined in (1.7) in terms of the single vertical scale z . The evolution of q in (5.1) is governed by the potential vorticity equation in (1.6).

The second issue regarding the non-invertibility of $\Delta - 3L$ and the description of freely-propagating $2f_0$ waves is addressed by applying the map $\partial_t \mapsto -2if_0 + \partial_{\bar{t}}$ to (3.24) through (3.27) prior to deriving (3.29). This procedure installs a time-derivative in the $2f_0$ evolution equation (3.29) and fixes its resonance problem. We leave the details for appendix A and report the resulting modified $2f_0$ equation:

$$(\Delta + 13L) B_t + 4if_0(\Delta - 3L)B = -\frac{3}{2}(\partial_x - i\partial_y)^2(LA)^2. \quad (5.3)$$

Non-dimensionalizing (5.3) in the manner of section 2.1 reveals that $(\Delta + 13L)B_t$ is ϵ^2 smaller than the rest of equation (5.3). The small term $(\Delta + 13L)B_t$ becomes important under conditions of near-resonance when $4if_0(\Delta - 3L)B$ is relatively small.

The expansion of ∂_t used to derive equation (5.3) is an application of the ‘method of reconstitution’ (Roberts 1985). Reconstitution successfully improves many asymptotic expansions, including the Navier-Stokes equations. Here, reconstitution of $2f_0$ dynamics by addition of the high-order term $(\Delta + 13L)B_t$ empowers (5.3) to describe freely-propagating $2f_0$ waves.

6. Conservation laws

Like XV, we find that the wave-averaged system (1.6) through (1.9) conserves two integral quantities, which we call ‘wave action’ and ‘coupled energy’.

6.1. Wave action

The first conservation law follows from the wave equations (1.8) and (1.9). We multiply (1.8) with $\frac{1}{2}LA^*$, add the complex conjugate, and integrate over the domain. Using the $2f_0$ equation (5.3), and a liberal application of integration by parts, we find

$$\frac{d}{dt} \int \frac{1}{2}|LA|^2 + \frac{1}{6}|\nabla B|^2 + \frac{13f_0^2}{6N^2}|B_z|^2 dV = 0. \quad (6.1)$$

The appearance of the B -terms in this first conservation law is a consequence of the time derivative in the $2f_0$ equation (5.3) and corresponds to the *total* energy in the freely propagating part of the near- $2f_0$ wave field. The conservation law (6.1) thus implies that resonant generation of propagating $2f_0$ waves extracts near-inertial kinetic energy.

6.2. Coupled energy

The second conserved quantity is a wave-mean coupled energy. We derive the associated conservation law by multiplying the potential vorticity equation (4.1) with ψ and integrating over the domain. The Jacobian term $\psi J(\psi, q)$ can be written as an exact derivative and integrates to zero. Applying integration by parts, we are left with

$$\frac{d\mathcal{E}_\psi}{dt} = \int \psi q_t^w dV, \quad (6.2)$$

where q^w is the wave potential vorticity defined in (4.2) and

$$\mathcal{E}_\psi \stackrel{\text{def}}{=} \int \frac{1}{2}|\nabla\psi|^2 + \frac{1}{2}\frac{f_0^2}{N^2}\psi_z^2 dV \quad (6.3)$$

is the total balanced quasi-geostrophic energy. Next we multiply (1.8) by $iLA_t^*/2f_0$, add the complex conjugate, and integrate over the domain to obtain

$$\frac{d\mathcal{E}_f}{dt} = - \int \psi q_t^w dV - \frac{i}{2f_0} \int B^* \partial_t \partial_s^2 (LA)^2 - B \partial_t \partial_{s^*}^2 (LA^*)^2 dV, \quad (6.4)$$

where

$$\mathcal{E}_f \stackrel{\text{def}}{=} \int \frac{f_0^2}{4N^2} |\nabla A_z|^2 + \frac{\beta y}{2f_0} |LA|^2 dV \quad (6.5)$$

is the sum of NIW potential energy and an action-like term associated with the β -effect. The first term on the right of (6.4) corresponds to the term on the right of (6.2) and will cancel when these equations are added. Substitution of the $2f_0$ equation (1.9) and its complex conjugate into the second integral on the right of (6.4) followed by persistent integration by parts produces

$$\frac{d\mathcal{E}_{2f}}{dt} = \frac{i}{2f_0} \int B^* \partial_t \partial_s^2 (LA)^2 - B \partial_t \partial_{s^*}^2 (LA^*)^2 dV, \quad (6.6)$$

where

$$\begin{aligned} \mathcal{E}_{2f} &\stackrel{\text{def}}{=} \int \frac{i}{12f_0} \left[B(\Delta + 13L) B_t^* - B^*(\Delta + 13L) B_t \right] - \frac{1}{3} |\nabla B|^2 + \frac{f_0^2}{N^2} |B_z|^2 dV, \\ &= \int \frac{i}{8f_0} \left[B^* (\partial_x - i\partial_y)^2 (LA)^2 - B (\partial_x + i\partial_y)^2 (LA^*)^2 \right] + \frac{1}{3} |\nabla B|^2 - \frac{f_0^2}{N^2} |B_z|^2 dV. \end{aligned} \quad (6.8)$$

An additional substitution of equation (1.9) and its complex conjugate transforms equation (6.7) into (6.8). The conservation of coupled energy emerges from the combination of (6.2), (6.4), and (6.6),

$$\frac{d}{dt} (\mathcal{E}_\psi + \mathcal{E}_f + \mathcal{E}_{2f}) = 0. \quad (6.9)$$

The conservation law in (6.9) is identical to XV's except for addition of the \mathcal{E}_{2f} term. Equation (6.9) is the analog of a conservation law found by Danioux *et al.* (2015) that relates the evolution of NIW potential energy to advection and refraction by steady geostrophic flows.

A thought experiment due to XV illuminates an important implication of (6.9): envision the rapid and stormy deposition of a horizontally-extensive, surface-concentrated current in a region of geostrophic turbulence. As the storm passes, the unbalanced current develops into surface-concentrated NIW which is almost horizontally-uniform, and therefore has little potential energy and thus $\mathcal{E}_f \approx 0$. Over subsequent inertial periods, NIW refraction and advection by the geostrophic flow drives the creation of near-inertial horizontal scales and potential energy, which leads to vertical propagation of a refracted NIW signal and the generation of $2f_0$ internal waves. Because wave action in (6.1) and coupled energy in (6.9) are distinct and independent conservation laws, total NIW and $2f_0$ wave energy increases in this process at the sole expense of energy in the geostrophic flow. The role of \mathcal{E}_{2f} in (6.9) is unfortunately obscure in this thought experiment, though the diagnosis of (6.9) presented in figure 7 below shows the effect is minor in some cases.

7. Comparison of three-component model and Boussinesq equations

To build confidence in the heuristic and asymptotic approximations used to develop the three-component model, we compare numerical solutions of a two-dimensional initial

value problem in the three-component model and the Boussinesq equations. The initial problem is similar to that shown in figure 1, in which a surface-concentrated NIW interacts with a barotropic balanced velocity field. In addition to solutions intended for direct comparison, we compute solutions to a two-component model without $2f_0$ dynamics, and a three-component model with the PSI-like part of NIW- $2f_0$ interaction removed. The physical implications of the numerical solutions are discussed in section 8.

7.1. A surface-concentrated near-inertial wave in random barotropic flow

The initial value problem involves the interaction of a surface-concentrated NIW with random, barotropic balanced flow. The two-dimensional physical domain is bounded by rigid lids in z with height $H = 4$ km and is periodic in x with width $L = 800$ km. The stratification is uniform with buoyancy frequency $N = 2 \times 10^{-3} \text{ s}^{-1}$ and the inertial frequency is $f_0 = 10^{-4} \text{ s}^{-1} = N/20$ with $\beta = 0$. As for the problem considered in section 1, the NIW initial condition is

$$LA(x, z, 0) = u(x, z, 0) = U_0 \exp(-z^2/2h^2), \quad (7.1)$$

with $h = 100$ meters. We consider initial NIW surface velocities of $U_0 = 0.4, 0.2$ and 0.1 m/s.

The initial, balanced v -velocity is

$$\psi_x(x, z, 0) = v(x, z, 0) = V_0 \sum_{n=4}^{14} \left(\frac{k_4}{k_n} \right)^{-2} \cos(k_n x + \phi_n), \quad (7.2)$$

where $k_n \stackrel{\text{def}}{=} 2\pi n/L$ and the ϕ_n are random phases between 0 and 2π for each component of the geostrophic flow. We choose $V_0 = 0.1 \text{ m s}^{-1}$ for all simulations. This produces a maximum velocity of $\max(v) \approx 0.2 \text{ m s}^{-1}$, a maximum Rossby number of $\max(v_x)/f_0 \approx 0.1$ and root-mean-square Rossby number of $\text{rms}(v_x)/f_0 \approx 0.05$. The balanced flow and its associated vorticity field are plotted at the top of figures 2 through 4.

The numerical solutions we report are listed in table 7.1. We choose simulation parameters both for ease of numerical integration and for consistency with oceanic scenarios. In particular, $V_0 = 0.1 \text{ m s}^{-1}$ leads to ‘reasonable’ NIW vertical propagation in ten or twenty of inertial periods; smaller values of V_0 lead to slower vertical propagation. Note however that $V_0 = 0.1 \text{ m s}^{-1}$ violates assumptions made in section 2 to justify the asymptotic derivation of the three-component model: the expansion assumes that $\bar{U}/\tilde{U} = \tilde{H}/\bar{H} = \epsilon \ll 1$. In the following simulations $\tilde{H}/\bar{H} = \pi h/H = 0.08 \ll 1$ while $\bar{U}/\tilde{U} = V_0/U_0$ ranges between 0.25 and 1, so that the balanced flow seems too strong given that the non-dimensionalization in section 2.1 assumes $\tilde{H}/\bar{H} \sim \bar{U}/\tilde{U} = \epsilon \ll 1$. Nevertheless we find generally good agreement between the predictions of the three component model and full Boussinesq solutions. Other calculations with V_0 reduced to 0.025 m s^{-1} not shown here also validate the three-component model.

We note finally that our two-dimensional computations do not test all aspects of the three component model: with $\partial_y = 0$ the advective terms $J(\psi, LA)$ and $J(\psi, q)$ vanish and the APV q does not evolve from its initial distribution. The two-dimensional simulations reported here are interesting primarily as a test of the nonlinear NIW- $2f$ interaction and the associated production of small vertical scales. Probing the advective terms requires either three-dimensional solutions like those in Danioux *et al.* (2008) or solutions of the two-dimensional model introduced in section 6.2 of XV.

TABLE 1. Parameters and models for numerical simulations reported in sections 7 and 8. A resolution of ‘1×’ is $n_x \times n_z = 1024 \times 2048$ and ‘2×’ is twice that. In all runs $\psi_x^q = v(t=0)$ is given by (7.2) with $V_0 = 0.1$ m/s.

U_0 (m/s)	Resolution	Model(s)	Notes
0.4	1× and 2×	Boussinesq and three-component model	
0.4	1×	Two-component model with $B \mapsto 0$	‘no $2f_0$ ’
0.2	1×	Boussinesq and three-component model	
0.2	1×	Two-component model with $B \mapsto 0$	‘no $2f_0$ ’
0.2	1×	Equations (7.3), (7.5), and (7.4) with $B_{xx}LA^* \mapsto 0$	‘no PSI’
0.1	1×	Boussinesq and three-component model	

7.2. Methods

In two dimensions, the APV equation (1.6) reduces to $q_t = 0$ and implies that q is constant. We decompose the balanced streamfunction into $\psi(x, z, t) = \psi^q(x, z) + \psi^w(x, z, t)$, where

$$(\partial_x^2 + L) \psi^q = q, \quad \text{and} \quad (\partial_x^2 + L) \psi^w = -\frac{1}{4f_0} \partial_x^2 |LA|^2. \quad (7.3)$$

Like q , ψ^q is constant in time and determined by the initial condition. Because LA is initially uniform, we have $\psi^q = \psi(t=0)$ and thus $\psi_{xx}^q = v_x(t=0)$. With this decomposition the two-dimensional three-component system becomes

$$LA_t + \frac{i}{2} f_0 A_{xx} + \frac{i}{2} (\psi_{xx}^q + \psi_{xx}^w) LA + \frac{1}{2} B_{xx} LA^* = -D(LA), \quad (7.4)$$

$$(\partial_x^2 + 13L) B_t + 4i f_0 (\partial_x^2 - 3L) B + \frac{3}{2} \partial_x^2 (LA)^2 = -D(LB), \quad (7.5)$$

where the linear ‘‘hyperdiffusion’’ operator

$$D \stackrel{\text{def}}{=} \nu \left[\left(\frac{\delta x}{\delta z} \right)^2 \partial_x^2 + \partial_z^2 \right]^8 \quad (7.6)$$

helps ensure numerical stability. In (7.6) ν is the hyperviscosity and $(\delta x, \delta z)$ is the resolution in (x, z) . We set $\nu = 10^6$ m¹⁶/s for all simulations reported here and find that the fractional energy lost to dissipation is negligible.

Equations (7.3) through (7.5) are solved with a pseudospectral method by decomposing A and B into the constant- N vertical modes $\cos(n\pi z/H)$ in z , and Fourier modes in x . Fast Fourier transforms are used for vertical and horizontal modal projections. Time integration of (7.4) and (7.5) is performed with the exponential time differencing method described by Cox & Matthews (2002), Kassam & Trefethen (2005), and Grooms & Julien (2011). The exponential time differencing method is crucial for integrating (7.4) and (7.5) efficiently due to the stiffness generated by both hyperdiffusion at small scales and the term $(\partial_x^2 - 3L)B$ in (7.5) at large scales.

A subtlety of the vertical mode decomposition of A emerges because we set the barotropic, vertically-uniform modes of A to zero. For the vertically-uniform and x -dependent parts of A , this helps ensure that w_0 in (3.8) vanishes at top and bottom boundaries. However, the vertically- and horizontally-uniform part of A does not have this constraint: this ‘domain mode’ corresponds to a pure inertial oscillation with no spatial

structure or evolution that exactly solves the volume-integrated Boussinesq equations in (2.2) through (2.6). The domain mode might be regarded as a covert and constant ‘fourth component’ that can be eliminated by posing an initial condition with no net momentum. In the results presented here the complex velocity of the domain mode is $e^{-if_0 t} (HL)^{-1} \int LA(x, z, 0) dx dz$, where $LA(x, z, 0)$ is the initial NIW amplitude given in (7.1). Because the domain mode is included in our Boussinesq solutions, we add it to the horizontal velocity of the numerical solution of (7.4) and (7.5) shown in figures 2 and 8. The domain mode makes a small but discernible impact on the solution at $t = 10$ in figure 2.

The nonhydrostatic Boussinesq equations in (2.2) through (2.6) with $\beta = 0$ are solved with the model of Winters *et al.* (2004), which employs a pseudospectral method with Fourier horizontal modes, sine vertical modes for w, b , cosine vertical modes for u, v , and an integrating factor method with a 3rd-order Adams-Bashforth scheme for time-stepping.

We use the same order of hyperdiffusion for three-component and Boussinesq models. Non-exhaustive trial and error indicates our three-component code is stable with time-steps at least 10 times larger than those demanded by Winters’ Boussinesq model. The simulations reported here use 1024 Fourier modes in x and 2048 vertical cosine modes in z . To test dependency on resolution, we ran simulations with double the resolution for $U_0 = 0.4$ m/s in both Boussinesq and three-component models. The results are almost identical for the two resolutions.

7.3. Points of comparison

We use horizontal velocity, vertical velocity, and domain-integrated vertical kinetic energy to compare Boussinesq and three-component models. Because v is initially balanced, the unbalanced part of v is approximately isolated with

$$\delta v(x, z, t) = v(x, z, t) - v(x, z, 0). \quad (7.7)$$

On the other hand, u is unbalanced because $p_y = 0$. We thus define the unbalanced horizontal ‘wave speed’ as

$$\text{wave speed} \stackrel{\text{def}}{=} \sqrt{u^2 + \delta v^2}. \quad (7.8)$$

The wave speed in (7.8) includes NIW and $2f_0$ components as well as a much smaller wave-induced mean component. In figure 2, we compare the wave speed from the Boussinesq solution with $|\tilde{\mathcal{U}}| \approx |\mathcal{U}_0 + \tilde{\mathcal{U}}_1|$ diagnosed from the three-component solution, where $\mathcal{U}_0 = e^{-if_0 t} LA$ and $\tilde{\mathcal{U}}_1$ is the wavy part of (3.31). The comparison is made at $t = 10, 40$, and 80 inertial periods. The initial NIW magnitude in figure 2 is $U_0 = 0.4$ m/s and the initial, balanced, barotropic v and local Rossby number v_x/f_0 are plotted in upper left and right panels.

The wave speed shown in figure 2 indicates good agreement between the three-component model and Boussinesq equations. A close inspection of the fields is required to discern differences that arise between the two models at late times. It is our consistent experience that the wave speed field is well-estimated by the three-component model for the two-dimensional initial value problems examined here; we therefore focus the following discussion on the more interesting and worst-case comparison of vertical velocity.

The vertical velocities in Boussinesq and three-component solutions are compared in figures 3 and 4 for initial NIW magnitudes $U_0 = 0.4$ and 0.2 m/s. Vertical velocity is plotted from top to bottom at $t = 10, 40$, and 80 inertial periods. For both cases, agreement is good at $t = 10$ inertial periods but degrades progressively thereafter. A

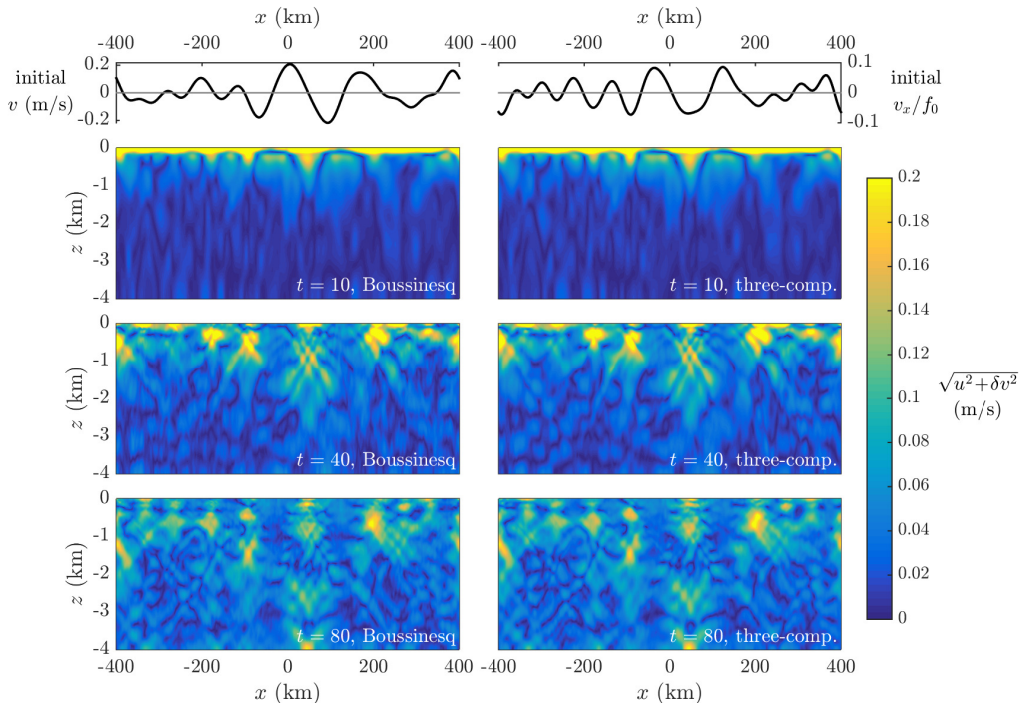


FIGURE 2. Comparison of wave speed in numerical solutions to the three-component and Boussinesq models. The top two panels show the x -dependence of the initial balanced velocity v (left) and balanced vorticity normalized by f_0 , v_x/f_0 (right). The lower three panels show wave speed defined in (7.8) at $t = 10, 40$, and 80 inertial periods in the Boussinesq model (left panels) and the three-component model (right panels). The initial NIW surface velocity is $U_0 = 0.4$ m/s.

conspicuous aspect of the Boussinesq solution absent from the three-component solution are features with small horizontal scales and steep characteristic angles. These features are especially prominent in figure 3 for the most nonlinear case with $U_0 = 0.4$ m/s at $t = 40$ and 80 inertial periods.

We dissect this failure of the three-component model in figure 5, which compares vertical kinetic energy (VKE) spectra between three-component and Boussinesq models for $U_0 = 0.4 \text{ m s}^{-1}$ at $t = 10$ and 40 inertial periods. The five lines indicate internal wave frequencies based on the linear dispersion relation; proceeding clockwise from the vertical axes these frequencies are $1.01f_0$, $1.08f_0$, $2f_0$, $3f_0$, and $4f_0$, with the dashed line corresponding to $2f_0$. The dynamics are clear: in the Boussinesq simulations, substantial VKE leaks into higher harmonic frequencies $3f_0$ and $4f_0$. By $t = 40$ inertial periods, the fraction of VKE contained in frequencies greater than $2.8f_0$ is 49%. This transfer of VKE to higher harmonics decreases with U_0 : for $U_0 = 0.2$ and 0.1 m s^{-1} , the fraction is 10% and just over 1%, respectively, at $t = 40$ inertial periods.

The effect of the energy transfer to NIW harmonics on total VKE is demonstrated in figure 6, which shows the evolution of total VKE, $\int w^2/2 \, dx \, dz$, for (a) $U_0 = 0.4 \text{ m s}^{-1}$ and (b) $U_0 = 0.2 \text{ m s}^{-1}$. Four models are considered: Boussinesq (solid lines), three-component model (dashed lines), a two-component model which neglects $2f_0$ (dash-dotted lines), and a modification of the three-component model with PSI suppressed by removing $B_{xx}LA^*$ from the NIW equation (7.4) (dotted line, figure 6(b) only). The three-component model

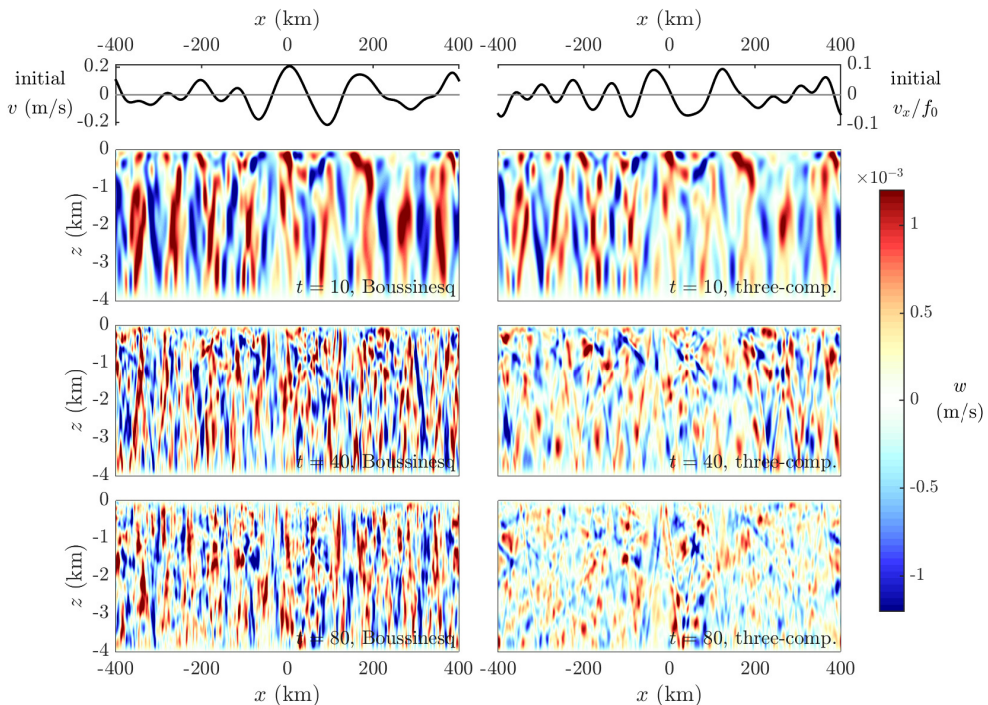


FIGURE 3. Comparison of vertical velocity in numerical solutions to the Boussinesq and three-component models. The top two panels show the x -dependence of initial v (left) and v_x/f_0 (right). The lower three panels show vertical velocity w at $t = 10, 40$, and 80 inertial periods for Boussinesq (left panels) and three-component model (right panels). The initial NIW surface velocity is $U_0 = 0.4$ m/s.

underestimates the amplitude of VKE, having 54% of the Boussinesq solution at $t = 40$ inertial periods and 43% of the total at $t = 80$ inertial periods. The ‘extra’ Boussinesq VKE is thus similar to that contained in frequencies greater than $2.8f_0$, implying that it originates in a transfer of horizontal NIW kinetic energy to high NIW harmonics not accounted for in the three-component model. It is not surprising that this transfer to $3f_0$ and $4f_0$ is strongest in the most nonlinear case with $U_0 = 0.4$ m/s⁻¹.

For the case $U_0 = 0.2$ m/s⁻¹ the three-component model correctly estimates the amplitude, but not the phase of VKE. Unsurprisingly, given the impact of NIW-harmonic interactions on VKE, the two-component solutions with $B \mapsto 0$ and thus no $2f_0$ cannot capture the evolution of VKE for either $U_0 = 0.4$ or 0.2 m/s⁻¹. In figure 6(b), the suppression of PSI leads to an unrealistic accumulation of VKE in $2f_0$ motions starting at around $t = 20$ inertial periods. This indicates that the transfer of energy from $2f_0$ back to NIWs must be accounted for to accurately capture VKE evolution.

7.4. Summary

The comparison presented in this section shows that the three-component model well-describes NIW evolution and nonlinear NIW- $2f_0$ interaction. That the three-component describes NIW evolution in the cases shown here is not too surprising, since it is likely driven by a linearized YBJ-type flow-induced refraction. The success of the three-component in describing NIW- $2f_0$ interaction is more surprising and vindicates the heuristic derivation of $2f_0$ dynamics. On the other hand, the model grossly under-

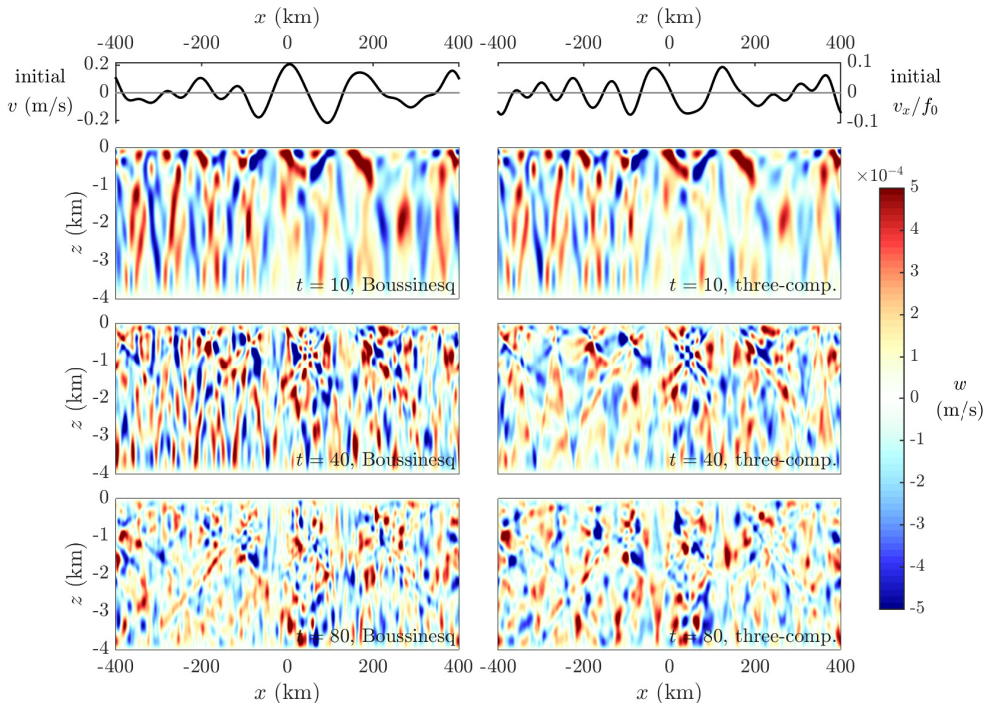


FIGURE 4. Like figure 3 but with initial NIW surface velocity $U_0 = 0.2$ m/s. The agreement between Boussinesq and three-component models is better than for $U_0 = 0.4$ m/s.

estimates vertical velocity magnitude when the NIWs are strong, which follows from the neglect of NIW harmonics higher than $2f_0$. We stress that this two-dimensional comparison cannot test whether the three-component model correctly captures the impact of NIWs on balanced flow evolution.

8. Energy transfer and production of small vertical scales

In this section we continue to explore the initial value problem of section 7 by looking at the energy transfer between the three flow components and the surprising role played by $2f_0$ in the evolution of the smallest vertical scales.

8.1. Energy transfer between flow components

The two conserved quantities in the three-component model are wave action and coupled energy defined in (6.1) and (6.9) and plotted in figure 7(a) and (b). Figure 7(a) illustrates the transfer between NIW kinetic energy and the total energy of the $2f_0$ field, defined respectively as

$$\mathcal{A}_f = \int \frac{1}{2} |\mathbf{L}\mathbf{A}|^2 dV \quad \text{and} \quad \mathcal{A}_{2f} = \int \frac{1}{6} |B_x|^2 + \frac{13f_0^2}{6N^2} |B_z|^2 dV. \quad (8.1)$$

Figure 7(a) shows the components of wave action change $\delta\mathcal{A}_f(t) \stackrel{\text{def}}{=} \mathcal{A}_f(t) - \mathcal{A}(0)$ and \mathcal{A}_{2f} . Figure 7(a) also shows the very small change in total wave action $\delta\mathcal{A} = \delta\mathcal{A}_f + \mathcal{A}_{2f}$ due to hyper-dissipation with dotted lines. All curves are normalized by initial wave action $\mathcal{A}(0)$, which is equal to the kinetic energy in the near-inertial initial condition. Three

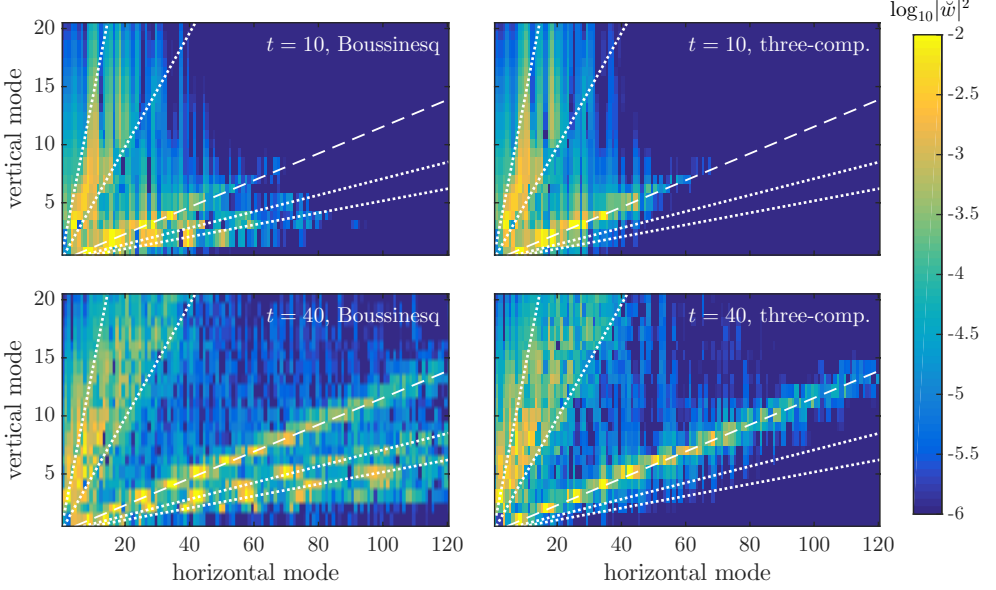


FIGURE 5. Snapshots of VKE spectral components, $|\tilde{w}|^2$, where \tilde{w} denotes the Fourier and vertical mode transform of w , for $U_0 = 0.4$ m/s at $t = 10$ and 40 inertial periods. The spectral components are normalized by total Boussinesq VKE and horizontal modes include energy from both positive and negative horizontal wavenumbers. The five lines show the linear dispersion relation for five internal wave frequencies; proceeding clockwise from the vertical axes these frequencies are $1.01f_0$, $1.08f_0$, $2f_0$, $3f_0$, and $4f_0$, with the dashed line corresponding to $2f_0$. By $t = 40$ inertial periods, 49% of the Boussinesq VKE is in frequencies higher than $2.8f_0$.

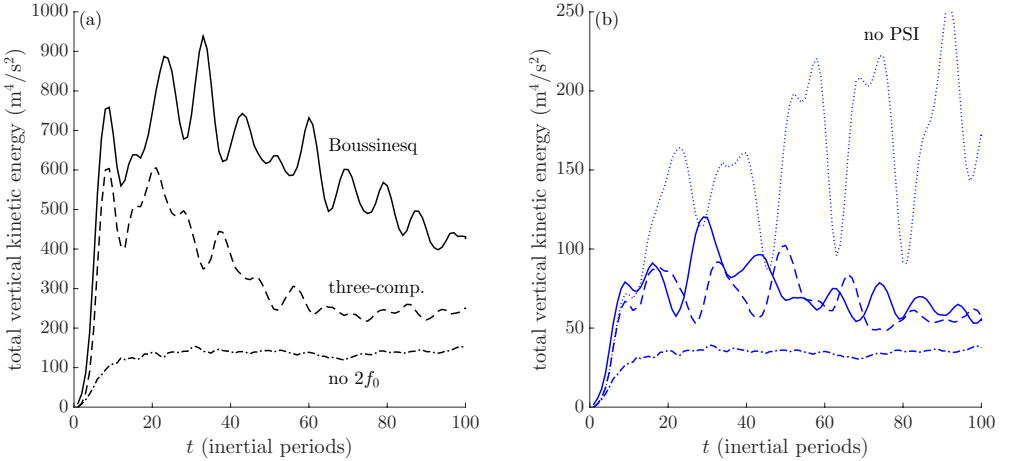


FIGURE 6. Evolution of total VKE $\int w^2/2 dx dz$ for (a) $U_0 = 0.4$ m/s and (b) $U_0 = 0.2$ m/s. Results are diagnosed from the Boussinesq model (solid lines), three-component model (dashed lines), a ‘no $2f_0$ ’ two-component model with $B \mapsto 0$ (dash-dotted lines), and a ‘no PSI’ three-component model with the term $B_{xx}LA^*$ removed from the NIW equation (7.4) (dotted line in panel (b) only). Black colors are used for (a) $U_0 = 0.4$ m/s and blue colors for (b) $U_0 = 0.2$ m/s here and in figures 7 and 9.

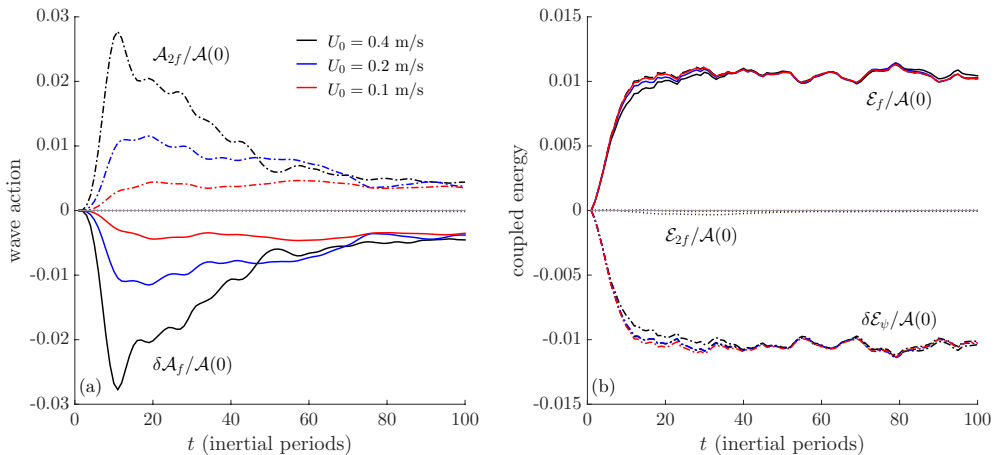


FIGURE 7. The evolution of (a) wave action and (b) coupled energy in the three-component system with initial NIW velocity in (7.1) and $U_0 = 0.4, 0.2$ and 0.1 m/s, and initial balanced velocity in (7.2) with $V_0 = 0.1$ m/s, as shown in figures 2 through 4.

cases corresponding to different initial amplitude of the NIW are shown: $U_0 = 0.1, 0.2$, and 0.4 m/s in red, blue, and black. The action transferred from \mathcal{A}_f to \mathcal{A}_{2f} increases initially to a maximum value and thereafter decays to a constant asymptotic value as $t \rightarrow \infty$. Although the short-term maximum transfer increases with the initial NIW amplitude U_0 , the fraction as $t \rightarrow \infty$ is independent of U_0 and indicates that less than 1% of the near-inertial action is ultimately transferred to the $2f_0$ field.

Figure 7(b) shows the evolution of $\delta\mathcal{E}_\psi(t) \stackrel{\text{def}}{=} \mathcal{E}_\psi(t) - \mathcal{E}(0)$, \mathcal{E}_f , and \mathcal{E}_{2f} following the definitions in (6.3), (6.5), and (6.7), respectively. All energies are normalized by the initial near-inertial kinetic energy $\mathcal{A}(0)$, thus revealing an uncanny correspondence between cases: the energy transferred from balanced flow to NIWs is a *constant fraction* of the initial NIW kinetic energy, $\mathcal{A}_f(0)$.

8.2. $2f_0$ motions are a stepping stone to small vertical scales

The evolution of \mathcal{A}_{2f} in figure 7(a) is unspectacular and suggests NIW- $2f_0$ interaction is not important because at most a mere 3% of the initial NIW kinetic energy is transferred to $2f_0$ when $U_0 = 0.4$ m/s. Yet the possibility for a PSI-type energy transfer from $2f_0$ to NIW hints that the inclusion of $2f_0$ and nonlinear NIW- $2f_0$ interaction may be necessary to capture the production of small NIW vertical scales.

We isolate the effect of this process by computing a ‘no $2f_0$ ’ solution of (7.3) and (7.4). In this solution we set $B \mapsto 0$, thus removing $2f_0$ waves and the $2f_0$ -mediated transfer of energy. Figure 8 gives a qualitative impression of the results, where wave speed (top panels) and wave shear magnitude (bottom panels) are plotted for three model solutions with $U_0 = 0.4 \text{ m s}^{-1}$: Boussinesq (left), three-component model (middle), and the two-component ‘no $2f_0$ ’ solution of equations (7.3) and (7.4) with $B \mapsto 0$ (right). Both Boussinesq and three-component results have small scales in the vertical velocity which are lacking when $2f_0$ is removed, and thus must be created by nonlinear NIW- $2f_0$ interaction. Without $2f_0$ the magnitude of vertical shear is also underestimated near $(x, z) = (-0.1, 40)$ km. At the same time, the overall flow structure agrees between the three models.

A more quantitative estimate of small vertical scales is provided by the metric $\text{Ri}^\dagger(t)$, which measures the smallest Richardson numbers and thus the potential for wave break-

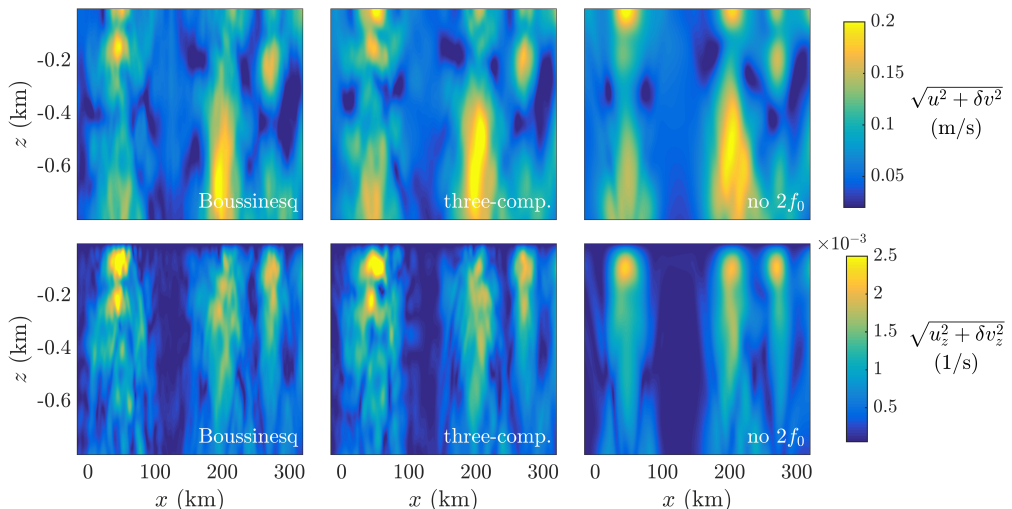


FIGURE 8. Comparison of velocity magnitude and shear magnitude between the Boussinesq equations, the three-component model, and a two-component model with $B \mapsto 0$ and thus no $2f_0$ waves. The snapshots are taken at $t = 80$ inertial periods and comprise a portion of the full domain shown in figure 2.

ing and mixing were such processes resolved. Ri^\dagger is defined as the average of the smallest 0.1% of Richardson numbers:

$$\text{Ri}^\dagger(t) \stackrel{\text{def}}{=} \text{mean}[\text{smallest 0.1\% of Ri values}], \quad \text{where} \quad \text{Ri} \stackrel{\text{def}}{=} \frac{N^2 + b_z}{u_z^2 + v_z^2}. \quad (8.2)$$

The evolution of Ri^\dagger normalized by its initial value is shown in figure 9 for the cases $U_0 = 0.4$ and 0.2 m/s. Results are compared between Boussinesq, three-component models, and two-component models. The comparison reveals that small values of Ri^\dagger and thus small vertical scales are produced by at least two distinct physical mechanisms. Ri^\dagger first decreases to a minimum value between $t = 15$ and 20 inertial periods and rises gradually thereafter. The early-time agreement between all five cases means that Ri^\dagger is controlled by refraction of the NIW field by balanced flow during this first stage.

However, at around $t = 40$ inertial periods, the results diverge and Ri^\dagger is smaller for $U_0 = 0.4$ m/s in both Boussinesq and three-component models. It is conspicuous that in the two-component model with $U_0 = 0.4$ m/s, Ri^\dagger is overestimated and stays close to the more linear $U_0 = 0.2$ m/s results. At this stage, the smallness of Ri^\dagger and thus small NIW vertical scales in Boussinesq and three-component models must be controlled by nonlinear NIW- $2f_0$ interaction. Strikingly, and despite that they contain little instantaneous energy, $2f_0$ motions provide a crucial stepping stone through which NIW energy is transferred to small vertical scales. The surprisingly accurate description of this process by the three-component model suggests it is controlled by the interaction of relatively large-vertical-scale $2f_0$ motions with small-scale NIWs, which figures 2 and 3 show are well-captured by the three-component model.

9. Discussion

We have developed a three-component model for the coupled evolution of near-inertial waves (NIWs), quasi-geostrophic (QG) flow, and internal waves with frequency near $2f_0$.

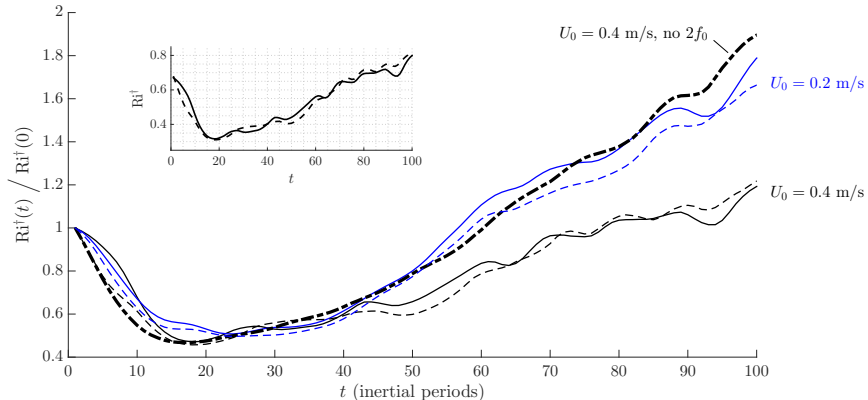


FIGURE 9. The evolution of Ri^\dagger defined in (8.2) and normalized by its initial value for the cases $U_0 = 0.4$ m/s (black) and $U_0 = 0.2$ m/s (blue or gray) and in three models: Boussinesq (solid lines), three-component model (dashed lines), and the two-component model with $B \mapsto 0$ and thus no $2f_0$ (dashed-dotted lines). The inset shows the numerical values of Ri^\dagger approaching the critical value $Ri = 1/4$ for the case $U_0 = 0.4$ m/s in Boussinesq and three-component models. Ri^\dagger is a measure of the smallest vertical scales in the flow, whose evolution cannot be captured without $2f_0$.

The three-component model adds $2f_0$ dynamics to the two-component NIW-QG model derived by Xie & Vanneste (2015), and thereby describes the prominent $2f_0$ vertical velocities and production of small NIW vertical scales that numerical solutions of the Boussinesq equations show are important features of the coupled evolution of NIWs and balanced flow.

A striking prediction of both the three-component model and XV’s two-component model is that forced oceanic NIWs extract energy from large-scale balanced flows. Because it requires externally-forced internal waves, XV call this mechanism ‘stimulated loss-of-balance’, distinguishing it from the spontaneous loss-of-balance that occurs without external forcing of waves. Stimulated loss-of-balance acts even in small Rossby number flows, and our numerical solutions suggest that energy transfer to NIWs increases with the strength of the externally-forced waves. Gertz & Straub (2009) showed that stimulated loss-of-balance can result in a forward energy cascade and dissipation of wind-driven gyres in an unstratified thin aspect ratio fluid. The significance of stimulated loss-of-balance in real ocean flows is uncertain.

The three-component model connects the $2f_0$ generation mechanism identified by Danioux & Klein (2008) with the YBJ-based near-inertial PSI mechanism of Young *et al.* (2008). The form of the NIW- $2f_0$ coupling implies a two-step cycle for NIW energy: first, advection and refraction by balanced flow catalyzes transfer of NIW energy to $2f_0$ waves. These newly-produced $2f_0$ waves have large, often depth-spanning vertical scales and propagate rapidly in the horizontal. Second, a PSI-like interaction transfers energy from $2f_0$ waves back to the NIW field at very small vertical scales. This two-step process provides a path from the large scales of NIW forcing to the small scales of wave breaking and mixing. Advection and refraction of NIWs by non-uniform QG flows leads to relatively small NIW horizontal scales and thus plays a catalytic role in activating this path. Interestingly, the rapid horizontal and vertical propagation of the nascent $2f_0$ waves can excite small-scale NIWs in regions remote from the initial NIW forcing. Two-dimensional numerical solutions of both three-component and Boussinesq models give tentative confirmation of this mechanism.

The numerical comparison with the Boussinesq equations shows that strengths of the three-component model include its description of NIW refraction by balanced flow, and prediction of both the phase and amplitude of growing $2f_0$ waves at short times. A weakness of the three-component model is the underestimation of vertical velocity and vertical kinetic energy under increasingly nonlinear conditions due to its neglect of $3f_0$ - and $4f_0$ -frequency NIW harmonics. Despite this shortcoming, the three-component model captures with surprising accuracy the long-time evolution of the very smallest NIW vertical scales that result from nonlinear NIW- $2f_0$ interaction.

The numerical comparison primarily tests the accuracy of NIW- $2f_0$ dynamics in the three-component model in a regime where refraction by APV-induced balanced flow controls the large-scale NIW evolution. The magnitude of APV and the APV-induced flow means our comparison is not well-suited to isolate the existence and impact of balanced flow induced by quadratic NIW terms in (1.7). In addition, because APV cannot evolve from its initial condition in our two-dimensional scenario, the comparison cannot explore dynamic NIW-QG interaction. A three-dimensional comparison of three-component and Boussinesq dynamics is required to define the regimes of validity of the three-component model in more realistic scenarios and to unravel the effects of NIWs and their wave-induced balanced flow on the evolution of oceanic QG motion.

The applicability of the three-component model to a particular part of the ocean can be assessed using kinetic-energy frequency spectra derived from long-term mooring observations of horizontal velocity. Where non-wave flows of NIW-scale have small Rossby number, the three-component model well approximates the dynamics of any motion with *Eulerian* frequencies near f_0 . In flows with relative vorticities near or greater than f_0 , or under conditions of active wave breaking, the relevance of the three-component model is uncertain. The ubiquitous appearance of a spectral peak at f_0 combined with the belief that large, NIW-scale vortical flows are predominantly balanced (Ferrari & Wunsch 2009) hints at, but does not confirm, the potentially broad applicability of the three-component model. Such confirmation requires further observations, such as the difficult simultaneous observation of large-scale balanced vorticity and storm-driven NIW evolution. The applicability of the three-component model to real flows is of consequence because predicting the climatic evolution of diapycnal mixing likely requires a firm understanding of near-inertial wave physics — a link between the large and small scales of oceanic motion.

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Appendix A. The $2f_0$ equation

In this appendix, we outline the asymptotic and heuristic steps that lead to the $2f_0$ equation in (1.9) and (5.3).

A.1. $2f_0$ -frequency forcing at first order

The vertically-averaged, time-fluctuating part of the first-order Boussinesq system in (3.24) through (3.27) is

$$\widehat{\mathcal{U}}_{1\bar{t}} + \mathrm{i}f_0 \widehat{\mathcal{U}}_1 + 2\tilde{p}_{0s^*} = -\mathrm{e}^{-2\mathrm{i}f_0\bar{t}} \widehat{\mathcal{J}}_2, \quad (\text{A } 1)$$

$$\tilde{p}_{0\bar{z}\bar{t}} + \widehat{w}_0 N^2 = 0, \quad (\text{A } 2)$$

$$\widehat{\mathcal{U}}_{1s} + \widehat{\mathcal{U}}_{1s^*}^* + \widehat{w}_{0\bar{z}} = 0, \quad (\text{A } 3)$$

where the wavy part of the leading-order pressure \tilde{p}_0 does not depend on the fast scale \bar{z} . The system above describes hydrostatic internal waves of general aspect ratio driven by the $2f_0$ -forcing on the right of (A 1).

A bit of wrangling with equations (A 1) through (A 3) leads to a single equation for the wavy part of the leading-order pressure field:

$$\partial_{\bar{t}} [\partial_{\bar{t}}^2 \bar{\mathbf{L}} + f_0^2 (\Delta + \bar{\mathbf{L}})] \tilde{p}_0 = 3\mathrm{i}f_0^3 \left(\mathrm{e}^{-2\mathrm{i}f_0\bar{t}} \widehat{\mathcal{J}}_{2s} - \mathrm{e}^{2\mathrm{i}f_0\bar{t}} \widehat{\mathcal{J}}_{2s^*}^* \right). \quad (\text{A } 4)$$

Equation (A 4) is the hydrostatic internal wave equation forced at frequency $2f_0$. Writing \tilde{p}_0 as

$$\tilde{p}_0 = \mathrm{i}f_0 \left(\mathrm{e}^{-2\mathrm{i}f_0\bar{t}} B(x, y, \bar{z}, \bar{t}) - \mathrm{e}^{2\mathrm{i}f_0\bar{t}} B^*(x, y, \bar{z}, \bar{t}) \right), \quad (\text{A } 5)$$

and noting that (3.16) implies

$$\widehat{\mathcal{J}}_2 = \partial_s \widehat{M_{\bar{z}}^2}, \quad (\text{A } 6)$$

we find that B satisfies

$$\mathrm{i}f_0 (\Delta - 3\bar{\mathbf{L}}) B = -\frac{3}{2} \partial_s^2 \widehat{M_{\bar{z}}^2}. \quad (\text{A } 7)$$

A.2. Resonant and near-resonant NIW- $2f_0$ interaction

Equation (A 7) describes forced oscillations with frequency $2f_0$. It cannot describe the resonant and near-resonant generation and free propagation of $2f_0$ internal waves. Near-resonant generation can be understood by projecting (A 7) onto vertical modes $\mathbf{h}_n(z)$ which satisfy

$$\mathbf{L}\mathbf{h}_n + \kappa_n^2 \mathbf{h}_n = 0, \quad \text{and} \quad \mathbf{h}'_n = 0 \quad \text{at top and bottom}, \quad (\text{A } 8)$$

where the eigenvalue κ_n is the Rossby deformation wavenumber of mode n . If we look for solutions of the form $B \sim \mathrm{e}^{\mathrm{i}kx + \mathrm{i}\ell y}$, we find that (A 7) cannot be solved when

$$k^2 + \ell^2 = 3\kappa_n^2. \quad (\text{A } 9)$$

These combinations, which are circular slices of (k, ℓ) -space at each vertical mode, are the wavenumber combinations that satisfy the linear internal wave dispersion relation at frequency $2f_0$. Freely-propagating $2f_0$ internal waves are generated when the NIW forcing $\partial_s^2 \widehat{M_{\bar{z}}^2}$ has non-zero spectral content near these wavenumber combinations. The generality of near-resonant $2f_0$ generation in NIW-balanced flow interaction is evident from the results in figure 1 and the simulations in Danioux *et al.* (2008).

As resonant generation is generic, we seek to describe it by modifying equation (A 7). In particular, we need a term proportional to $B_{\bar{t}}$ in (A 7) in order to describe time-dependent B -generation and free near- $2f_0$ propagation. We achieve this by applying the map

$$\partial_t \mapsto -2\mathrm{i}f_0 + \partial_{\bar{t}}, \quad (\text{A } 10)$$

to (A 4) and re-deriving the $2f_0$ equation.

The scaling in section 2.1 implies that $\partial_{\bar{t}}$ is ϵ^2 smaller than $2f_0$; thus in applying (A 10) to (A 4) we ignore the even smaller $O(\epsilon^4)$ terms. Introducing (A 5) into the result then yields

$$-(\Delta - 11\bar{L}) B_{\bar{t}} + 2if_0 (\Delta - 3\bar{L}) B = -3\partial_s^2 \widehat{M_z^2}. \quad (\text{A } 11)$$

The leftmost term is ϵ^2 smaller than $(\Delta - 3\bar{L})B$ and only becomes important when $(\Delta - 3\bar{L})B \approx 0$. Moreover, the addition of any multiple of $(\Delta - 3\bar{L})B_{\bar{t}}$ does not reduce the ‘accuracy’ of the approximation in (A 11).

We exploit this ambiguity to improve the already-approximate form of (A 11). Consider the exact, vertical mode- n dispersion relation for linear hydrostatic internal waves,

$$\Sigma = \pm f_0 \sqrt{1 + \frac{k^2}{\kappa_n^2}}, \quad (\text{A } 12)$$

where $\Sigma(k, \kappa_n)$ is the hydrostatic internal wave frequency, k is the horizontal wavenumber, and κ_n is the horizontal wavenumber of the n^{th} vertical mode. The Taylor expansion of the positive root of Σ around $k = \sqrt{3}\kappa_n$ with κ_n fixed is

$$\Sigma = 2f_0 + \frac{\sqrt{3}f_0}{2\kappa_n} (k - \sqrt{3}\kappa_n) + \frac{f_0}{16\kappa_n^2} (k - \sqrt{3}\kappa_n)^2 + \dots. \quad (\text{A } 13)$$

On the other hand, the *approximate* dispersion relation implied by (A 11) is found by linearizing (A 11), projecting it onto vertical modes, and proposing $B \sim e^{ikx - i\sigma\bar{t}}$ so that the frequency of B is $2f_0 + \sigma$. Algebra reveals that $\Sigma_k = \sigma_k$ when $k = \sqrt{3}\kappa_n$ and $\Sigma = 2f_0$. As a consequence, the $2f_0$ approximation in (A 11) produces the correct group velocity.

This feature is preserved under the addition of any multiple of $(\Delta - 3\bar{L})B_{\bar{t}}$ to (A 11). We use this freedom to increase the accuracy of $2f_0$ linear dispersion in the three-component model: subtracting $\frac{9}{2}(\Delta - 3\bar{L})B_{\bar{t}}$ from (A 11), we obtain

$$(\Delta + 13\bar{L}) B_{\bar{t}} + 4if_0 (\Delta - 3\bar{L}) B = -6\partial_s^2 \widehat{M_z^2}. \quad (\text{A } 14)$$

The approximate dispersion relation implied by (A 14) is

$$\sigma = 4f_0 \frac{k^2 - 3\kappa_n^2}{k^2 + 13\kappa_n^2}, \quad (\text{A } 15)$$

which yields $\sigma_{kk} = \Sigma_{kk}$ and means that (A 14) produces the correct near- $2f_0$ group velocity over a range of wavenumbers. Figure 10 compares the exact dispersion relation with the approximate dispersion relations for both the $2f_0$ harmonic component as well as the NIW component, demonstrating the accuracy of our ‘Padé’ approximation to the $2f_0$ dispersion relation. We use equation (A 14) to model the $2f_0$ component of flow in the three-component system. Note too that such a ‘Padé’ approximation can be applied in the same manner to the NIW equation.

A.3. Expressions for \mathcal{U}_1 and \hat{w}_0

With \tilde{p}_0 defined through B , we can calculate $\tilde{\mathcal{U}}_1$. The vertically-averaged horizontal momentum equation is

$$\widehat{\mathcal{U}}_{1\bar{t}} + if_0 \widehat{\mathcal{U}}_1 = -2\tilde{p}_{0s^*} - e^{-2if_0\bar{t}} \widehat{\mathcal{J}}_2, \quad (\text{A } 16)$$

$$= -2if_0 e^{-2if_0\bar{t}} B_{s^*} + 2if_0 e^{2if_0\bar{t}} B_{s^*}^* - e^{-2if_0\bar{t}} \partial_s \widehat{M_z^2}. \quad (\text{A } 17)$$

which means that

$$\widehat{\mathcal{U}}_1 = e^{-2if_0\bar{t}} \left(2B_{s^*} - if_0^{-1} \partial_s \widehat{M_z^2} \right) + \frac{2}{3} e^{2if_0\bar{t}} B_{s^*}^*. \quad (\text{A } 18)$$

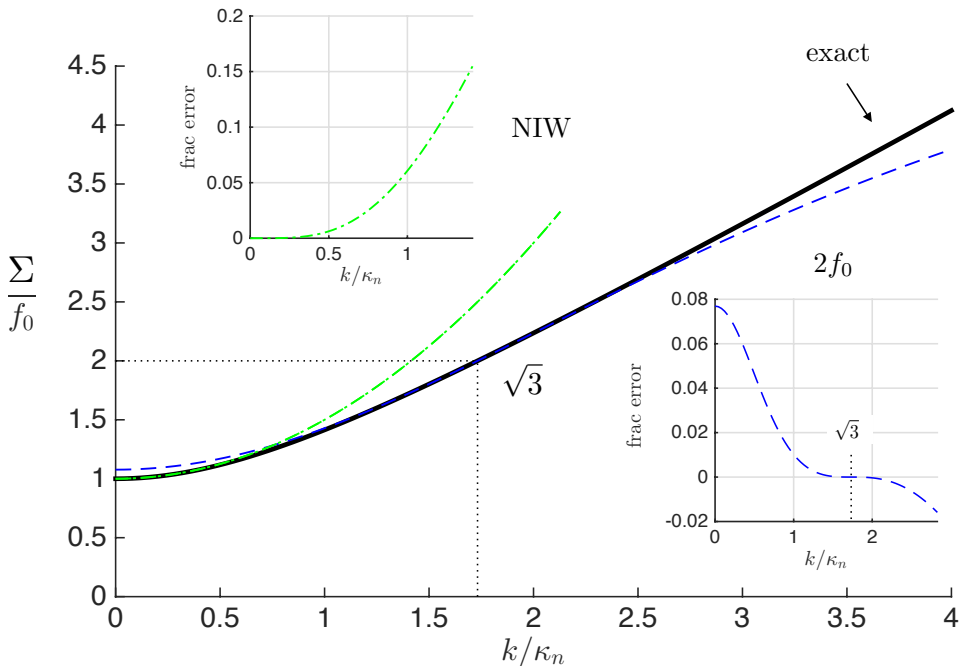


FIGURE 10. Comparison between the exact hydrostatic internal wave dispersion relation and the approximate linear dispersion relations in the three-component model. The thick black line traces the exact hydrostatic internal wave dispersion relation. The green dash-dotted line is the approximate dispersion relation for the NIW component, $f_0(1 + k^2/2\kappa_n^2)$, obtained by linearizing (1.8). The blue dashed line is the approximate dispersion relation for the $2f_0$ component implied by (1.9) and (A 14) and given by $2f_0 + \sigma$ in (A 15). Insets show the fractional error of the approximate NIW and $2f_0$ dispersion relations.

The vertically-averaged vertical velocity \hat{w}_0 is obtained from (A 2),

$$\hat{w}_0 = -\frac{2f_0^2}{N^2} \left(e^{-2if_0\tilde{t}} B_{\tilde{z}} + e^{2if_0\tilde{t}} B_{\tilde{z}}^* \right). \quad (\text{A } 19)$$

With \hat{w}_0 we can obtain the full expression for $\tilde{\mathcal{U}}_1$ by solving (3.24), which yields

$$\tilde{\mathcal{U}}_1 = e^{-2if_0\tilde{t}} (2B_{s^*} - if_0^{-1} \mathcal{J}_2) + \frac{2}{3} e^{2if_0\tilde{t}} B_{s^*}^* + \frac{f_0}{N^2} M_{\tilde{z}\tilde{z}} \left(e^{-3if_0\tilde{t}} B_{\tilde{z}} - e^{if_0\tilde{t}} B_{\tilde{z}}^* \right). \quad (\text{A } 20)$$

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